## Intrinsic thermoacoustic feedback and its consequences for combustion noise and combustion dynamics

**Wolfgang Polifke POLKA 4th Progress Meeting** April 28th 2022



Technische Universität München • Professur für Thermofluiddynamik



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## Thermoacoustic instabilities are a major challenge for combustion technology



### Liquid rocket engine (NASA 1957)



W. Polifke | Intrinsic thermoacoustic feedback | POLKA 4th Progress Meeting | April 2022



Liquid rocket engine (NASA 1963)

## The established paradigm of thermoacoustic instability: Unsteady flame heat release drives one of the acoustic cavity modes



A fluctuating flame is a monopole source of sound  $\rightarrow$  combustion noise or instability

Flame heat release rate responds to fluctuations of velocity with a time lag

 $\dot{Q}'(t) \leftarrow u'(t - \tau)$ 

Self-excited thermo-acoustic instability may result if phases  $p' \leftrightarrow \dot{Q}' \leftrightarrow u'$  are favorable



The flame impulse response h and the flame transfer function  ${\mathscr F}$  describe how flame heat release  $\dot{Q}'$  responds to velocity u'



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Polifke, PECS 2020

## The transfer matrix $\hat{T}$ of burner & flame links the flame transfer function $\mathscr{F}$ to up- and downstream acoustic variables u', p'



# $\begin{pmatrix} \frac{p'}{\rho c} \\ u' \end{pmatrix}_{I} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} \frac{p'}{\rho c} \\ u' \end{pmatrix}_{U}$

# The transfer matrix $\hat{T}$ of burner & flame links the flame transfer function $\mathscr{F}$ to up- and downstream acoustic variables u', p'





## The scattering matrix $\hat{S}$ provides an alternative description in terms of reflection and transmission coefficients for the characteristic wave f, g



# $\begin{pmatrix} f_d \\ g_{II} \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} J_u \\ g_d \end{pmatrix}$

## The scattering matrix $\hat{S}$ provides an alternative description in terms of reflection and transmission coefficients for the characteristic wave f, g



$$\begin{pmatrix} f_d \\ g_u \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix}$$

$$\begin{pmatrix} t_u & r_d \\ r_u & t_u \end{pmatrix}$$



## The scattering matrix $\hat{S}$ provides an alternative description in terms of reflection and transmission coefficients for the characteristic wave f, g



## Scattering matrix and instability potentiality of a premixed swirl burner show inexplicable peaks



Kunze, 2004, Fischer 2004, Gentemann & Polifke, ASME 2007; Polifke, ECM 2011

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## Scattering matrix and instability potentiality of a premixed swirl burner show inexplicable peaks



outgoing acoustic energy incoming acoustic energy

Kunze, 2004, Fischer 2004, Gentemann & Polifke, ASME 2007; Polifke, ECM 2011



## **Consequences of intrinsic thermoacoustic feedback** for combustion dynamics and combustion noise

Peaks in scattering matrix and instability potentiality

Thermoacoustic instability in anechoic system

ITA modes and resonances in real-world combustors

Anomalous behavior of ITA modes

l <sub>ud</sub>  $\mathsf{R}_{\mathsf{u}\mathsf{u}}$ C1  $R_{dd}$  $\omega$ **C**<sub>2</sub> du

Characteristic features of ITA modes

Exceptional points and clusters

+ = (8c)n (8c)d Th 1+2 2 N+2 Tan n 31 2 1+2  $\left(\frac{Td}{Th}-1\right)$ 1+2 1-2  $-\frac{1}{1+2+nF}$ fu 22 + 22 hF 1 + 8 + nF 1 - 2 + nF 1 + 2 + nF 1 + 2 + nFTAN gd fd an 95 Rn Sid. R2n 901 = 9 22+24Ff - 1-7 - - h Fa qu tot 50 1+2 96 190

Sebastian Bomberg, Thomas Emmert, May 30th, 2012

## Acoustic waves impinging upon the flame are transmitted / reflected





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## Unsteady heat release Q' contributes to the outgoing acoustic waves



## The flame heat release Q' is perturbed by upstream velocity $u_{u'}$



## The upstream velocity $u_u'$ is controlled by the upstream acoustics $f_u$ , $g_u$



## Acoustic waves generated by unsteady heat release Q' perturb the velocity $u_u$ ' upstream of the flame $\rightarrow$ intrinsic thermoacoustic feedback



## Analogy: electro-acoustic feedback









## Analogy: electro-acoustic feedback









## The peaks in $\hat{S}$ and the instability potentiality result from resonance with the ITA feedback loop



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## "Preventing thermo-acoustic instabilities by breaking the feedback loop" – does not work !?



Hoeijmakers et al., CNF 2014, 2016, Emmert et al, CNF, 2015

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Silva & Polifke, CNF, 2015



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## ITA feedback is important also if reflection coefficients are non-zero !



Emmert et al, PROCI 2017

### Re-arrange system matrix to segregate the network model into acoustic and ITA sub-systems, which may then be de-coupled

$$0 = \begin{bmatrix} -1 & \frac{Z_u + 1}{Z_u - 1} & 0 & 0 \\ \frac{\alpha - \xi}{\alpha + \xi} & -1 & 0 & \frac{2}{\alpha} \\ \frac{2\alpha\xi}{\alpha + \xi} & 0 & -1 & \frac{\xi - 1}{\alpha} \\ \frac{2\alpha\xi}{\alpha + \xi} & 0 & -1 & \frac{\xi - 1}{\alpha} \\ 0 & 0 & \frac{Z_d - 1}{Z_d + 1} & -1 \\ 1 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Emmert et al, PROCI 2017



## Re-arrange system matrix to segregate the network model into acoustic and ITA sub-systems, which may then be de-coupled

$$0 = \underbrace{\begin{bmatrix} -1 & \frac{Z_u + 1}{Z_u - 1} & 0 & 0 & 0 & 0 \\ \frac{\alpha - \xi}{\alpha + \xi} & -1 & 0 & \frac{2}{\alpha + \xi} & 0 & \frac{\theta}{\alpha + \xi} \\ \frac{2\alpha\xi}{\alpha + \xi} & 0 & -1 & \frac{\xi - \alpha}{\alpha + \xi} & 0 & \frac{\xi\theta}{\alpha + \xi} \\ 0 & 0 & \frac{Z_d - 1}{Z_d + 1} & -1 & 0 & 0 \\ 1 & -1 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & F & -1 \end{bmatrix}}_{u_u} \begin{bmatrix} f_u \\ g_u \\ f_d \\ g_d \\ u_u \\ \dot{q}' \end{bmatrix}$$







$$\begin{array}{c|ccccc} 0 & 0 & 0 \mu \frac{Z_u + 1}{Z_u - 1} \frac{\theta}{\alpha + \xi} \\ 0 & \frac{2}{\alpha + \xi} & 0 & 0 \\ -1 & \frac{\xi - \alpha}{\alpha + \xi} & 0 & \mu \frac{\xi \theta}{\alpha + \xi} \\ \frac{Z_d - 1}{1 + Z_d} & -1 & 0 & 0 \\ 0 & 0 & -1 & -\frac{\theta}{\alpha + \xi} \\ 0 & 0 & F & -1 \end{array} \begin{bmatrix} f_u \\ g_u \\ f_d \\ g_d \\ u_u \\ \dot{q}' \end{bmatrix}$$

 $ilde{A}(s)$ 

## Variation of the coupling coefficient $\mu$ : 1 $\rightarrow$ 0 associates a thermoacoustic mode with cavity *acoustics* or the *ITA* feedback loop



Emmert et al, PROCI 2017

### quarter wave mode

### ITA mode

### Helmholtz mode

## **Anomalous behaviour of the dominant ITA mode:** with *decreasing* reflection at the exit, $R_x = -1 \rightarrow 0$ its growth rate *increases*



Emmert et al, PROCI 2017

## One-way coupling between **combustion noise** source and combustor acoustics yields a resonance peak at 400 Hz - the quarter wave mode of the combustor



Silva et al, TIGRE, 2016, CNF 2017

## With two-way coupling, we recover also the low-frequency peak, and identify it as resonance of the noise source term with the ITA feedback loop



Silva et al, TIGRE, 2016, CNF 2017

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### Again, the ITA resonance peak shows non-intuitive response to variation in the exit reflection coefficient



Silva et al, TIGRE, 2016, CNF 2017

## For constant equivalence ratio, temperature, speed of sound the ITA peak frequency increases with flow speed – *convective scaling*



— 30 <i>kW</i>	11.3 <sup>m</sup> / <sub>s</sub>
— 50 kW	18.8 <sup>m</sup> / <sub>s</sub>
— 70 kW	26.4 <sup>m</sup> / <sub>s</sub>





## Convective scaling helped to identify a low frequency "bulk mode" in a spray flame combustor as an ITA mode



Eckstein et al., JPP, GTP, 2006



Ghani et al., CNF, 2019

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![](_page_41_Figure_11.jpeg)

## ITA modes seem to "interplay" with acoustic modes and change identity

![](_page_42_Figure_1.jpeg)

## Phasor analysis reveals the nature (ITA/acoustic) of marginally stable modes in an ideal resonator

![](_page_43_Figure_1.jpeg)

Yong et al., CNF, 2021

### Cavity modes sloshes back and forth across the heat source

![](_page_44_Figure_2.jpeg)

### ITA modes are 1D *push-pull* modes

![](_page_44_Figure_4.jpeg)

![](_page_44_Picture_5.jpeg)

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![](_page_45_Picture_8.jpeg)

![](_page_45_Figure_12.jpeg)

## With variation of flame parameters n, $\tau$ ITA modes and cavity modes interact at exceptional points

![](_page_46_Figure_1.jpeg)

Mensah et al., CNF, 2018 (see also Orchini et al., CNF, 2020)

![](_page_46_Figure_3.jpeg)

 $\mathcal{X}$ 

## The annular MICCA combustor exhibits acustic and clusters of ITA modes

![](_page_47_Figure_1.jpeg)

Buschmann et al., CNF, 2020

## **Publications**

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![](_page_48_Picture_13.jpeg)

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of Engineering for Gas Turbines and Power, vol. 134, 2012, pp. 21502-1-8.

![](_page_49_Picture_13.jpeg)

The complete set of thermoacoustic eigenmodes comprises cavity and ITA modes

ITA modes are characterized by a flip in u' and  $\nabla p'$  across the flame

ITA modes exhibit anomalous behaviour

ITA feedback explain paradoxical observations

TA analysis

![](_page_50_Picture_6.jpeg)

![](_page_50_Figure_9.jpeg)

The complete set of thermoacoustic eigenmodes comprises cavity and ITA modes

ITA modes are characterized by a flip in u' and  $\nabla p'$  across the flame

ITA modes exhibit anomalous behaviour

ITA feedback explain paradoxical observations

![](_page_51_Figure_5.jpeg)

## ITA feedback is important for instability / noise of open flames: Plate 4 has high viscous losses; unstable only at ITA frequency ~ 500 Hz

![](_page_52_Figure_1.jpeg)

## Dowling and Stow (JPP, 2003) observed in a low-order model of a gas turbine modes "associated with flame model"

![](_page_53_Figure_1.jpeg)

### ITA mode @ 168 Hz

![](_page_53_Figure_3.jpeg)

![](_page_53_Figure_4.jpeg)

![](_page_53_Picture_5.jpeg)