

Flame models for thermoacoustics

Maria Heckl and Sreenath M.Gopinathan
Keele University, UK

Outline

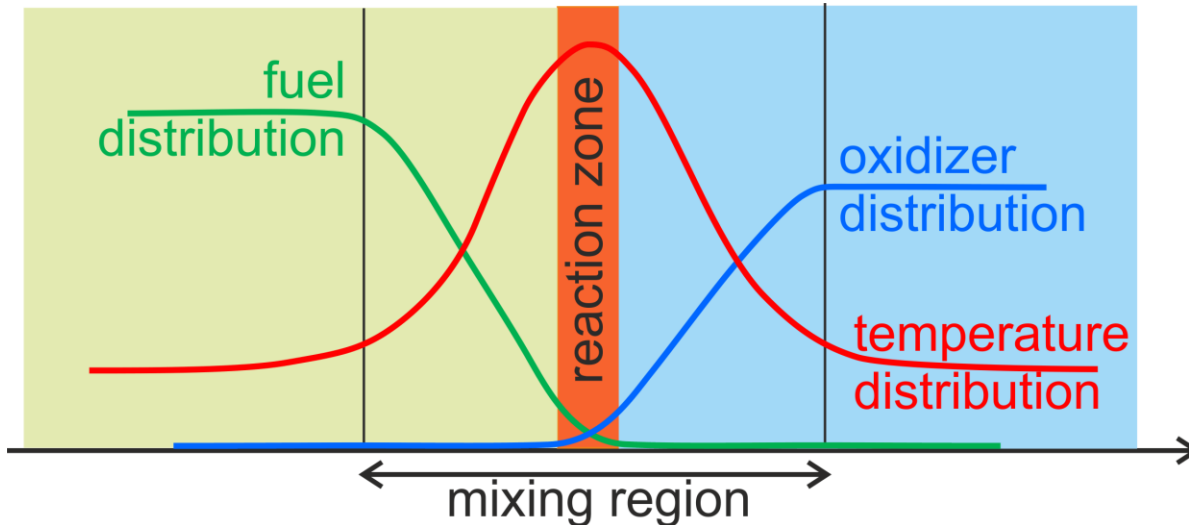
1. What is a flame?
2. The flame transfer function (FTF)
3. Impulse response of the flame
4. The flame describing function (FDF)
5. Flame modelling with the G-equation
6. Analytical approximation of a given FDF
7. Summary

1. What is a flame?

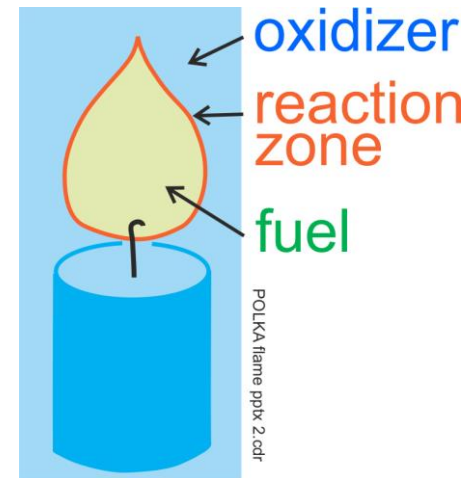
Combustion: fuel + oxidizer $\rightarrow$ burnt products + heat

Flame: visible part of combustion

1.1. Diffusion flame



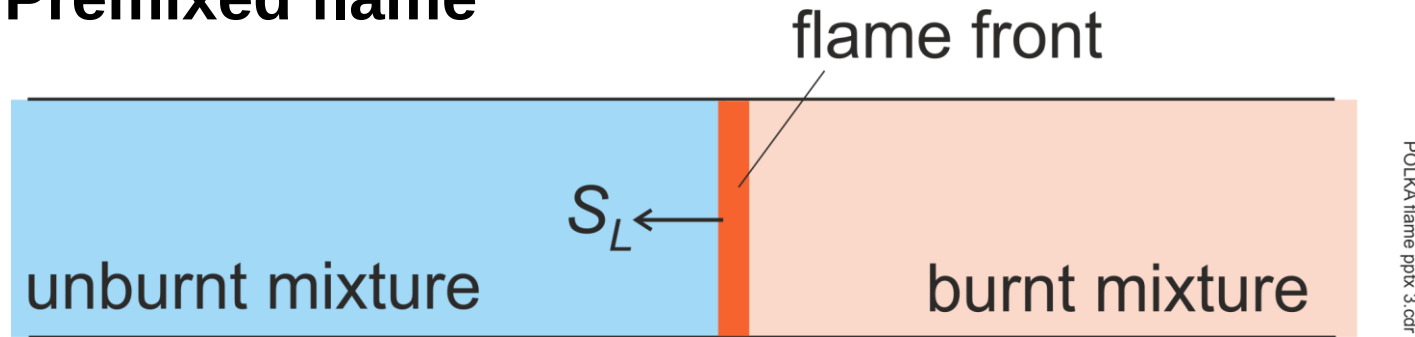
POLKA flame pptx 1.cdr



POLKA flame pptx 2.cdr

Reaction zone: fuel and oxidizer have similar concentration
not considered further

1.2. Premixed flame



S_L : **laminar flame speed**

propagation speed of flame relative to unburnt mixture

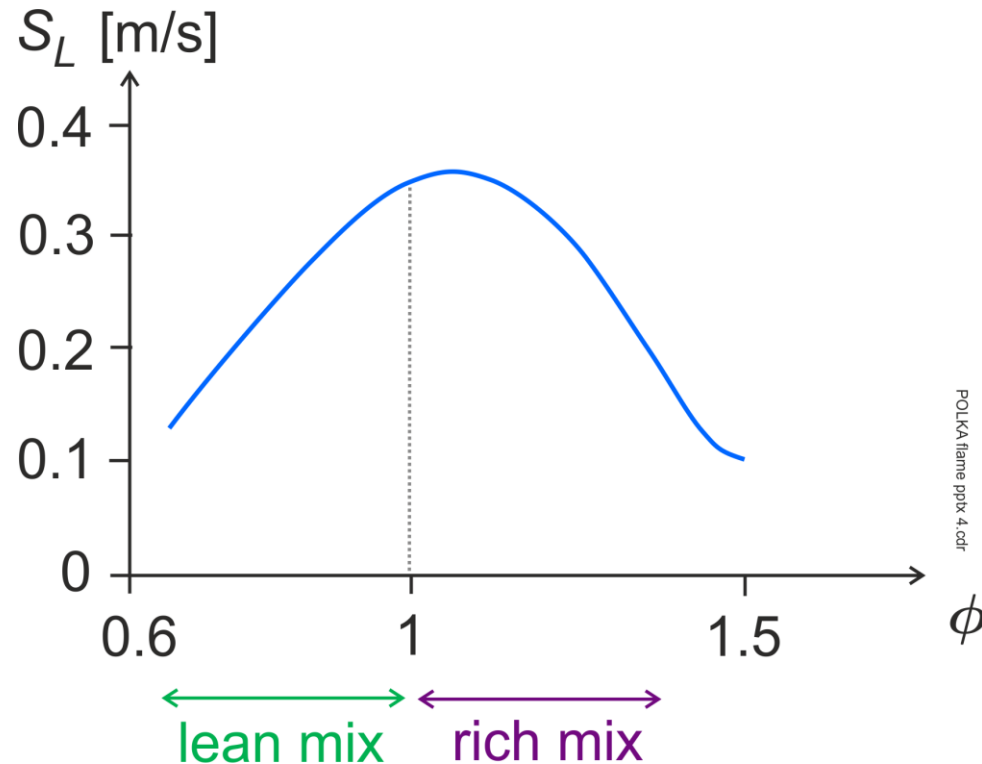
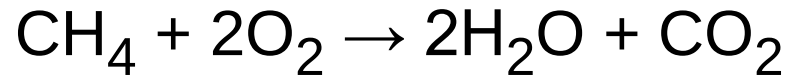
depends on fuel type and concentration.

concentration: $FO = \frac{\text{mass of fuel}}{\text{mass of } O_2}$

stoichiometric combustion: all fuel and all O_2 is consumed

equivalence ratio: $\phi = \frac{FO}{(FO)_{\text{stoichiometric}}}$

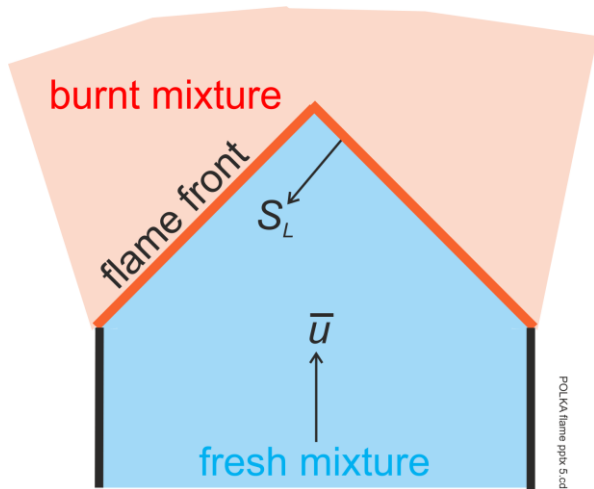
Example: Methane combustion



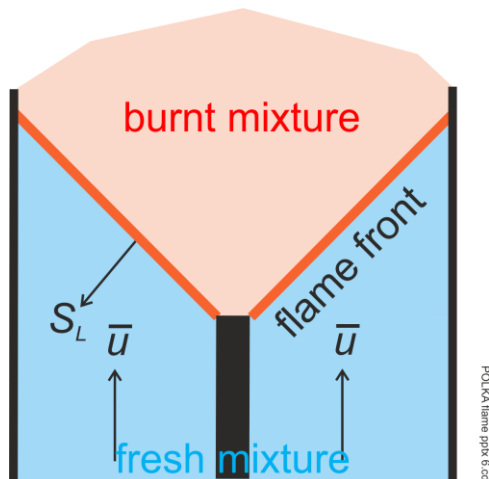
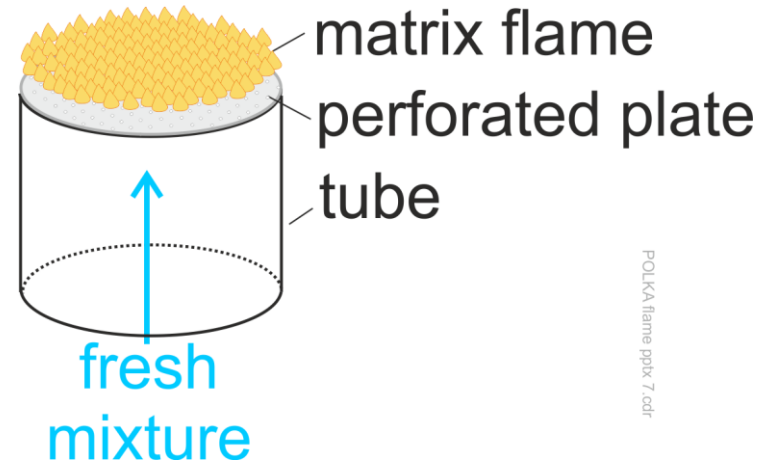
for hydrocarbons: $S_L = 0.1 - 0.5$ m/s

for hydrogen: $S_L = 0.5 - 10$ m/s

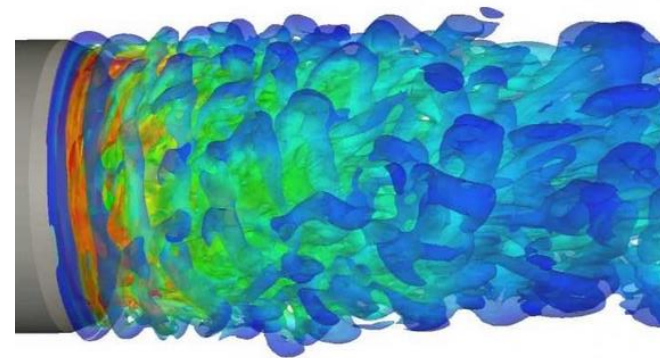
Examples of premixed flames



conical flame



V - flame



swirl flame

from:
<https://www.youtube.com/watch?v=jjLYE18wlp4>

2. The flame transfer function (FTF)

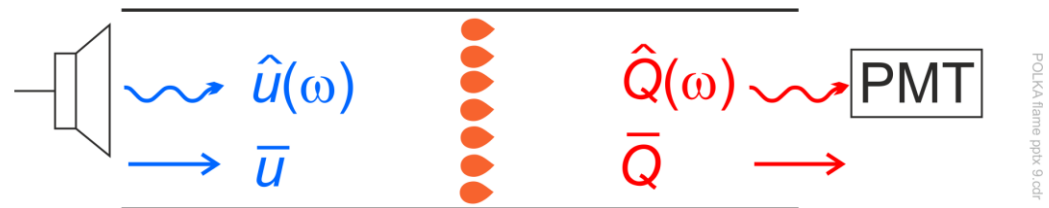
Consider the flame as an input-output system:



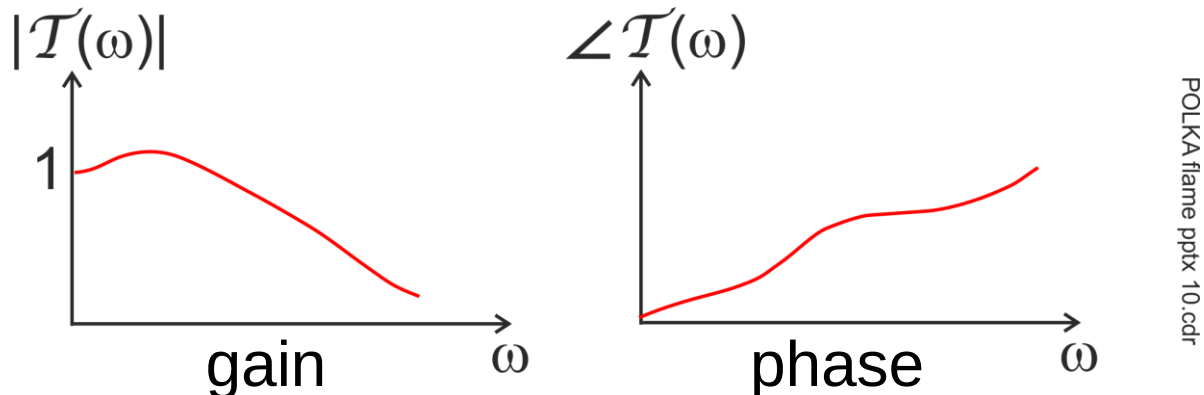
Definition of the FTF:

$$\mathcal{T}(\omega) = \frac{\hat{Q}(\omega) / \bar{Q}}{\hat{u}(\omega) / \bar{u}}$$

Measurement:



Typical result:



3. Impulse response of the flame

Apply inverse Fourier transform to $\frac{\hat{Q}(\omega)}{\bar{Q}} = \mathcal{T}(\omega) \frac{\hat{u}(\omega)}{\bar{u}}$

Result:
$$\frac{Q'(t)}{\bar{Q}} = \int_{-\infty}^{\infty} h(\tau) \frac{u'(t-\tau)}{\bar{u}} d\tau$$

inverse FT of $\mathcal{T}(\omega)$

Impulse response

input: $u'(t) = \bar{u} \delta(t)$ impulse

response:
$$\frac{Q'(t)}{\bar{Q}} = \int_{-\infty}^{\infty} h(\tau) \frac{\bar{u} \delta(t-\tau)}{\bar{u}} d\tau = h(t)$$

→ $h(t)$ is the impulse response.

$\mathcal{T}(\omega)$ and $h(t)$ contain the same physical information.

4. The flame describing function (FDF)

flame transfer function:
$$\mathcal{T}(\omega) = \frac{\hat{Q}(\omega) / \bar{Q}}{\hat{u}(\omega) / \bar{u}}$$

flame describing function:
$$\mathcal{T}(\omega, a) = \frac{\hat{Q}(\omega, a) / \bar{Q}}{\hat{u}(\omega, a) / \bar{u}}$$

Measurement:



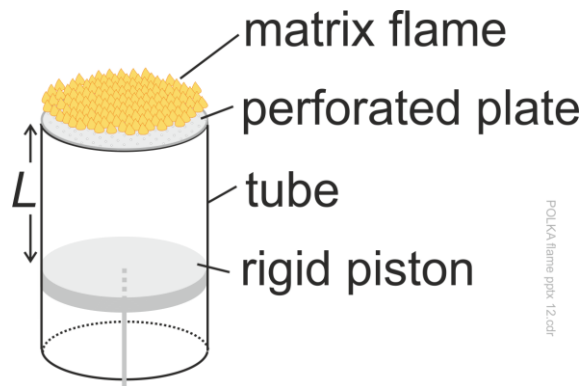
Frequencies other than ω in the output are ignored:



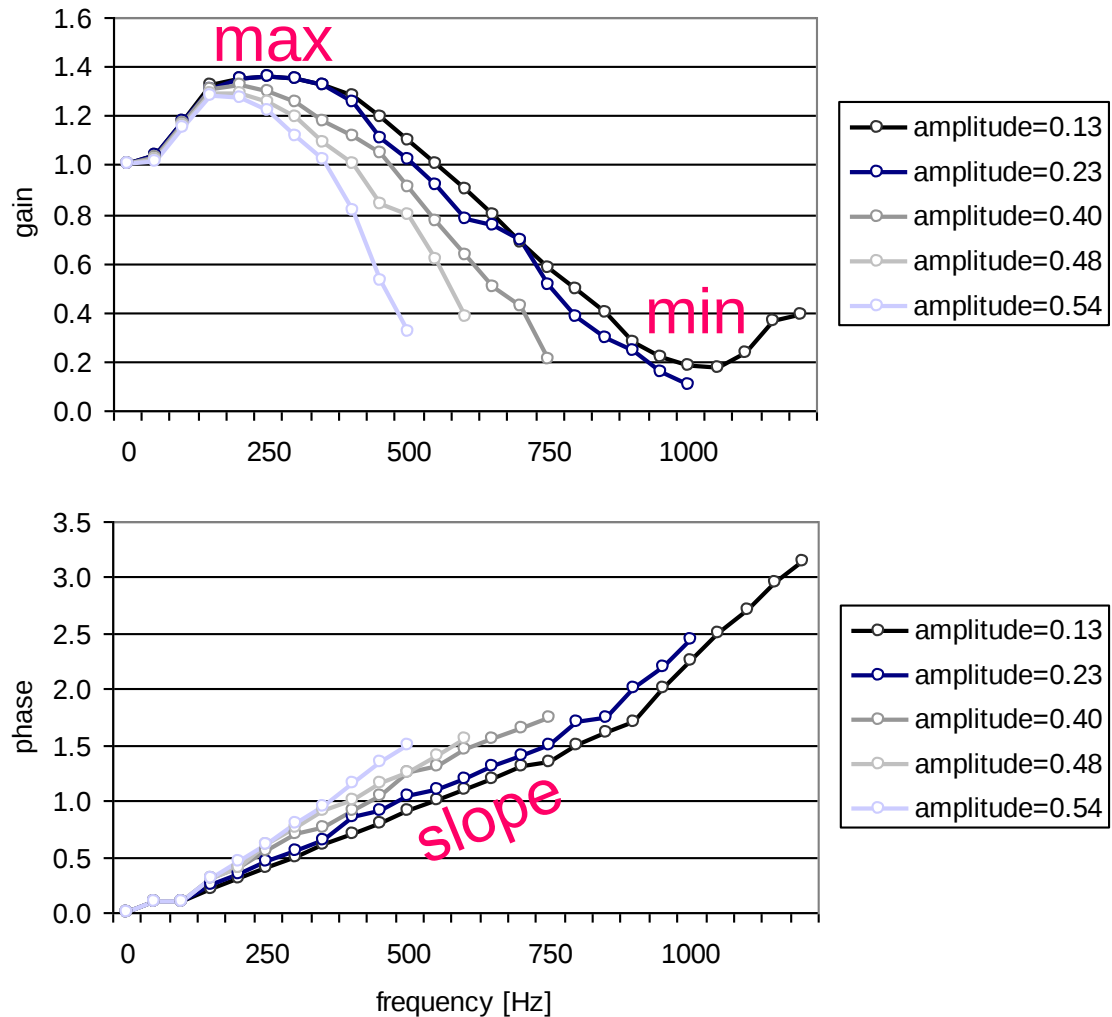
The inverse FT of the FDF is *not* the impulse response!

Example: FDF of Noiray's matrix flame

Noiray's test rig



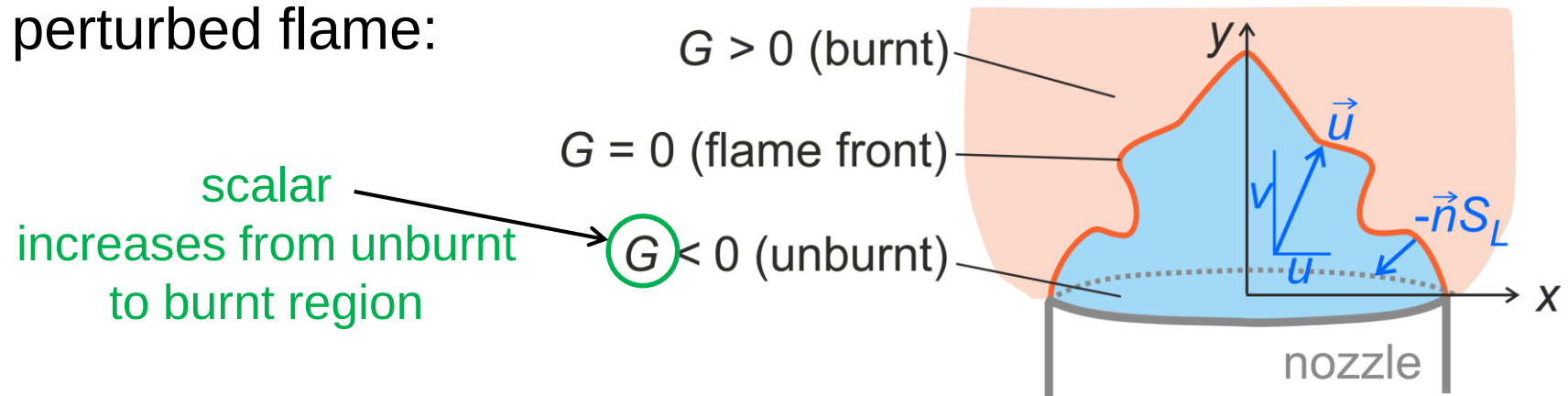
POLKA flame pptx 12.cdr



Noiray, N., Durox, D., Schuller, T. & Candel, S. (2008) A unified framework for nonlinear combustion instability analysis based on the flame describing function. *Journal of Fluid Mechanics* 615, 139-167.

5. Flame modelling with the G-equation

perturbed flame:



Flame surface: $G(\vec{x}, t) = 0$

Kinematic argument: convected derivative of G must be zero.

→ G-equation: $\frac{\partial G}{\partial t} + \vec{u} \cdot \nabla G = S_L |\nabla G|$

velocity field, excites the flame

Rotationally symmetric flame: $\vec{u} = \begin{pmatrix} u \\ v \end{pmatrix} = \vec{u}(x, y, t)$

$$\vec{u} \cdot \nabla G = u \frac{\partial G}{\partial x} + v \frac{\partial G}{\partial y}, \quad |\nabla G| = \sqrt{\left(\frac{\partial G}{\partial x}\right)^2 + \left(\frac{\partial G}{\partial y}\right)^2}$$

nonlinear term

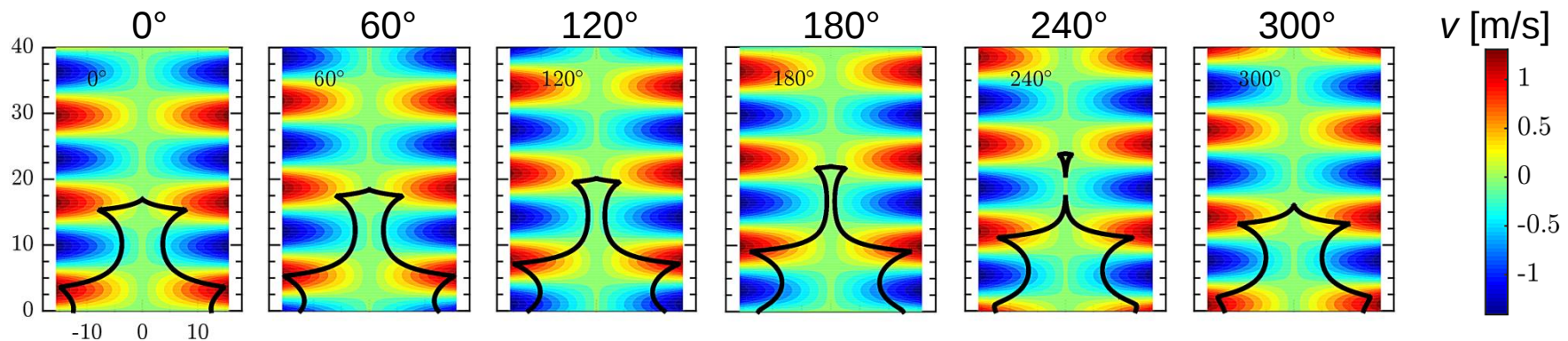
Assumption:

Excitation by velocity perturbation travelling with $\bar{u}$ mean flow velocity

$$u(x, y, t) = \bar{u} [1 + \varepsilon \sin(\omega t - ky)] \quad \text{with} \quad k = \omega / \bar{u}$$

$$v(x, y, t) \quad \text{from} \quad \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} = 0 \quad (\text{incompressible mass balance})$$

Numerical solution of G-equation $\rightarrow$ position of flame surface



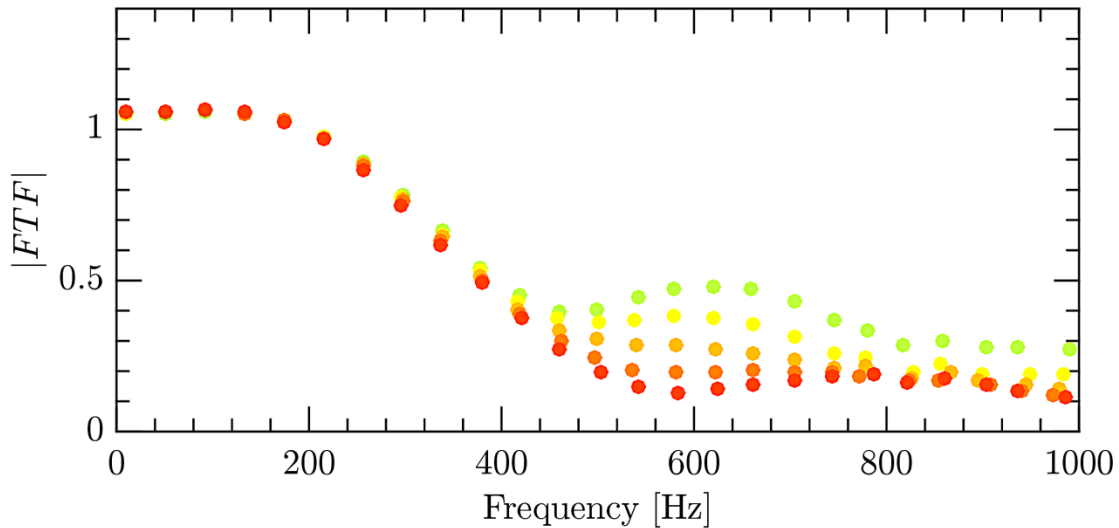
$\rightarrow$ flame surface area A

$\rightarrow$ rate of heat release ($Q \sim A$)

Repeat for various values of ε and $\omega \rightarrow$ FDF

FDF for a conical CH₄-H₂ flame

gain



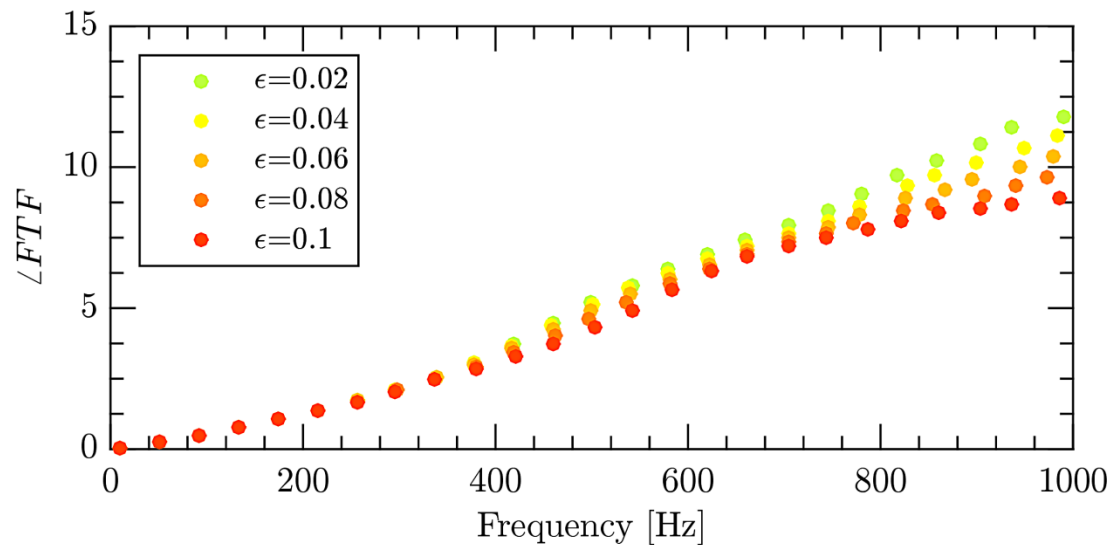
$$\phi=0.95$$

CH₄: 80%

H₂: 20%

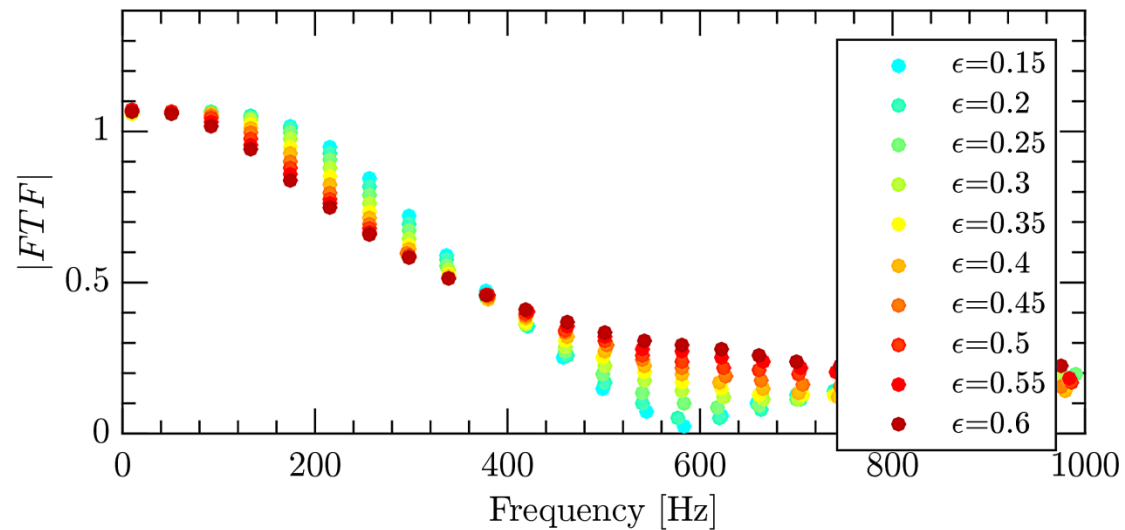
$$\epsilon = a / \bar{u}$$

phase

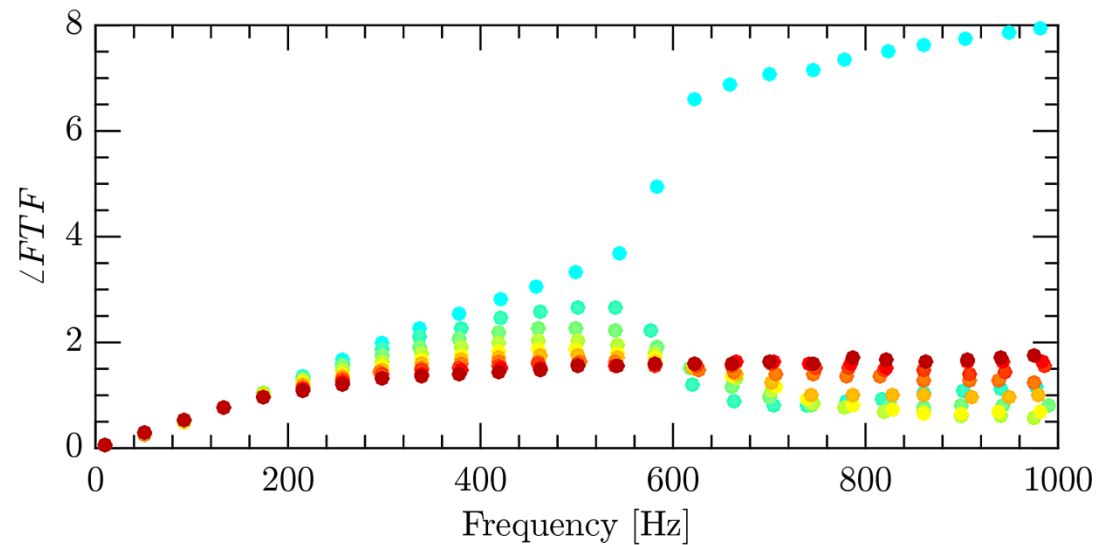


for higher amplitudes ($\epsilon = 0.15 \dots 0.6$):

gain



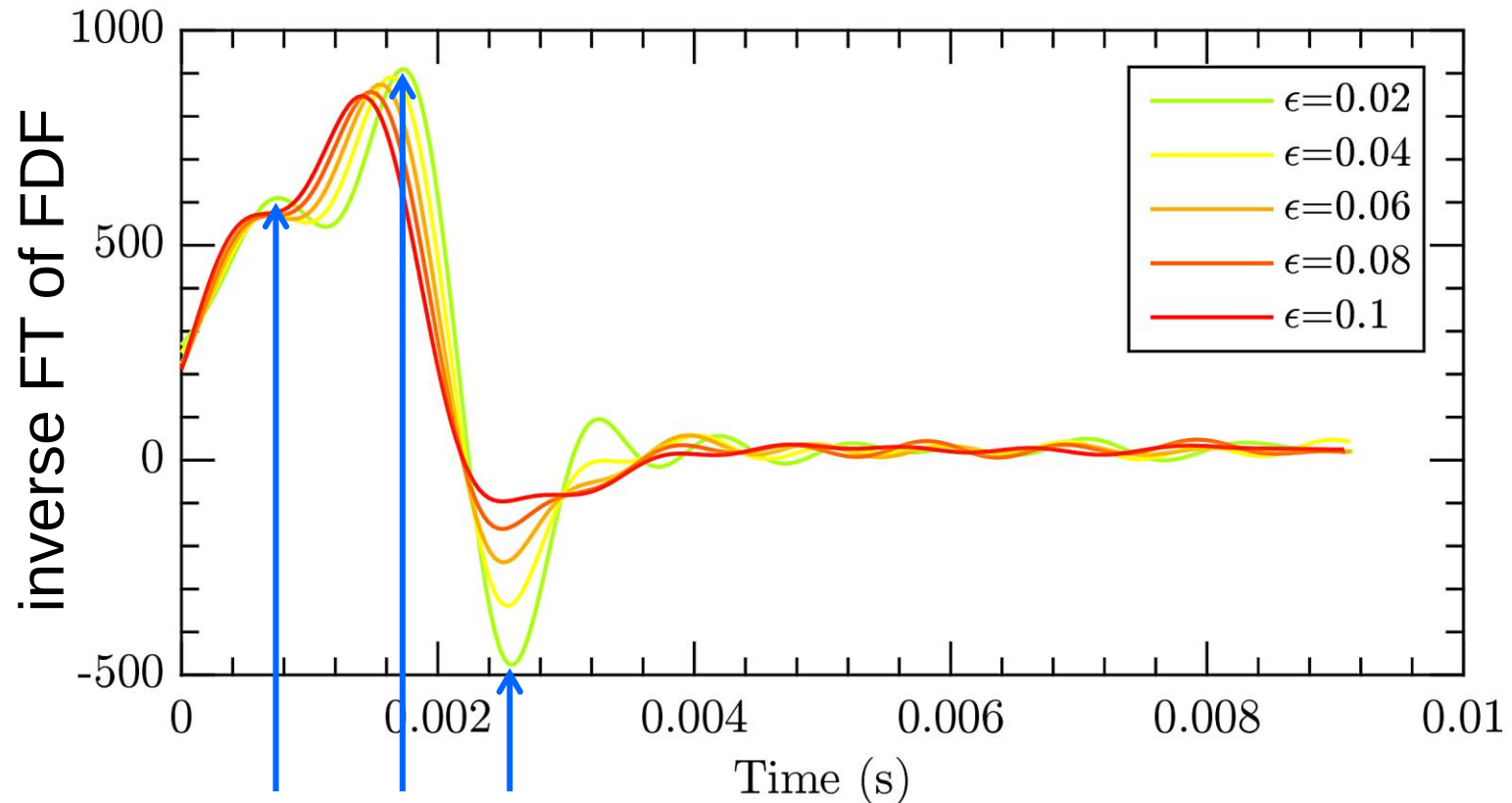
phase



6. Analytical approximation of a given FDF

6.1. Motivation and method

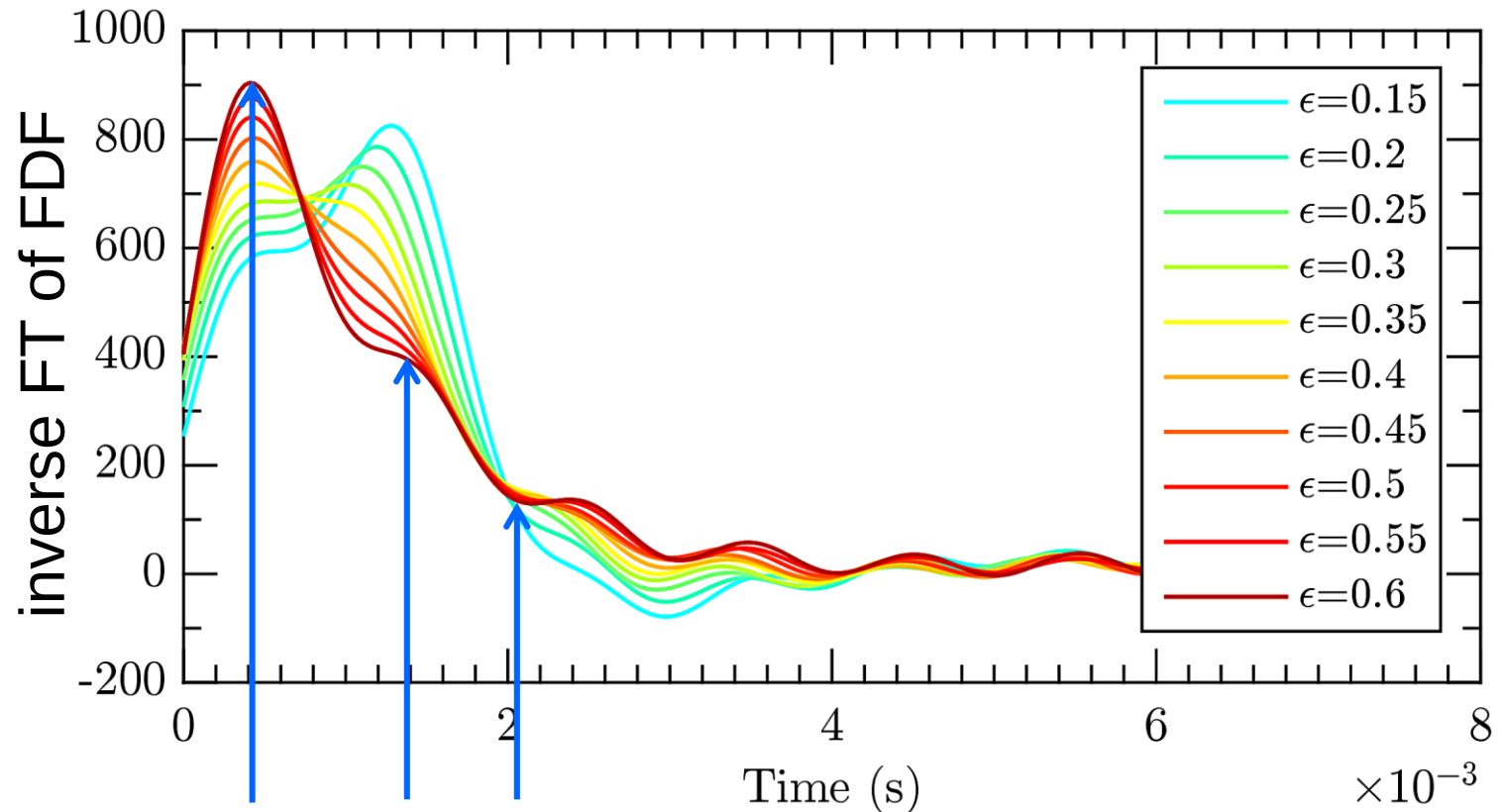
Inverse Fourier transform of FDF for the CH₄ - H₂ flame:



time lags: τ_1 τ_2 τ_3

surrounded by maxima/minima

for higher amplitudes ($\epsilon = 0.15 \dots 0.6$):



time lags: τ_1 τ_2 τ_3

surrounded by maxima/minima

Approximate dominant maxima/minima by Gauss curve:

$$\frac{n}{2\pi\sigma} e^{-\frac{(t-\tau)^2}{2\sigma^2}}$$

n : height of curve

σ : width of curve

τ : position of curve along time axis

superposition of Gauss curves:

$$\tilde{h}(t) = \frac{n_1}{2\pi\sigma_1} e^{-\frac{(t-\tau_1)^2}{2\sigma_1^2}} + \frac{n_2}{2\pi\sigma_2} e^{-\frac{(t-\tau_2)^2}{2\sigma_2^2}} + \frac{n_3}{2\pi\sigma_3} e^{-\frac{(t-\tau_3)^2}{2\sigma_3^2}}$$

$$(n_1, \tau_1, \sigma_1)$$

$$(n_2, \tau_2, \sigma_2)$$

...

amplitude-dependent fitting parameters

Determination of the fitting parameters

from simulation/experiment: $\mathcal{T}(\omega_i, a_k)$, $i = 1, 2, 3, \dots$ $k = 1, 2, 3, \dots$

apply inverse Fourier transform: $h(t_j, a_k)$, $j = 1, 2, 3, \dots$

approximate by $\tilde{h}(n_\ell, \tau_\ell, \sigma_\ell)$, $\ell = 1, 2, 3, \dots$

minimise the error $\left[h(t_j, a_k) - \tilde{h}(n_\ell, \tau_\ell, \sigma_\ell) \right]^2$

→ optimal fitting parameters $(n_\ell, \tau_\ell, \sigma_\ell)$

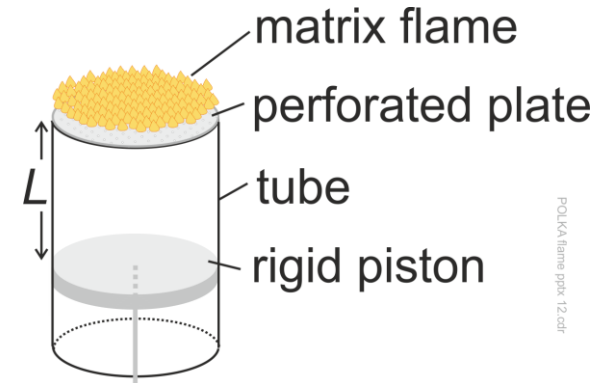
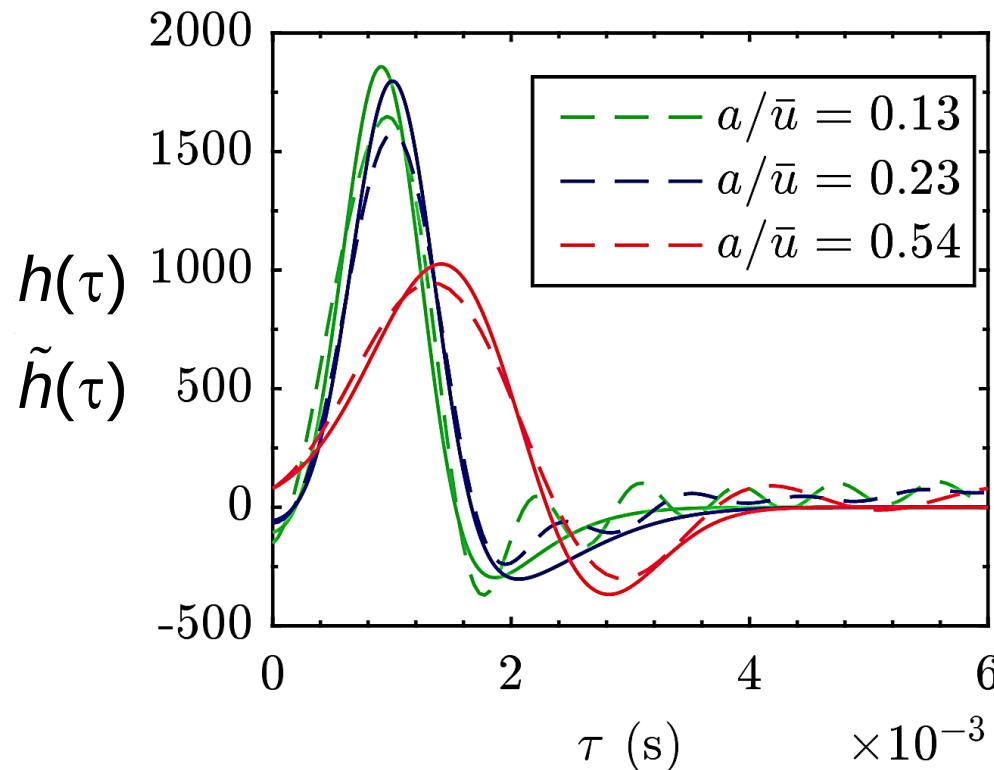
apply Fourier transform to optimal $\tilde{h}(n_\ell, \tau_\ell, \sigma_\ell)$
(can be done analytically)

→ $\tilde{\mathcal{T}}(\omega, a_k)$

analytical approximation for $\mathcal{T}(\omega_i, a_k)$

6.2. Application to Noiray's matrix flame

Results for $h(\tau)$ and $\tilde{h}(\tau)$



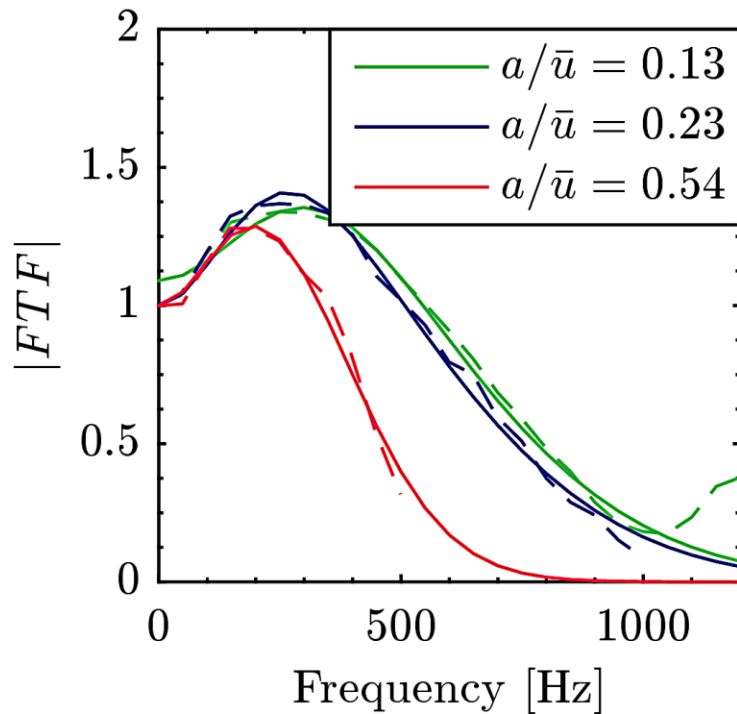
POLKA flame ppx 12.cdr

$\left. \begin{array}{l} \text{---} \text{---} \text{---} \\ \text{---} \text{---} \text{---} \\ \text{---} \text{---} \text{---} \end{array} \right\} h(\tau)$

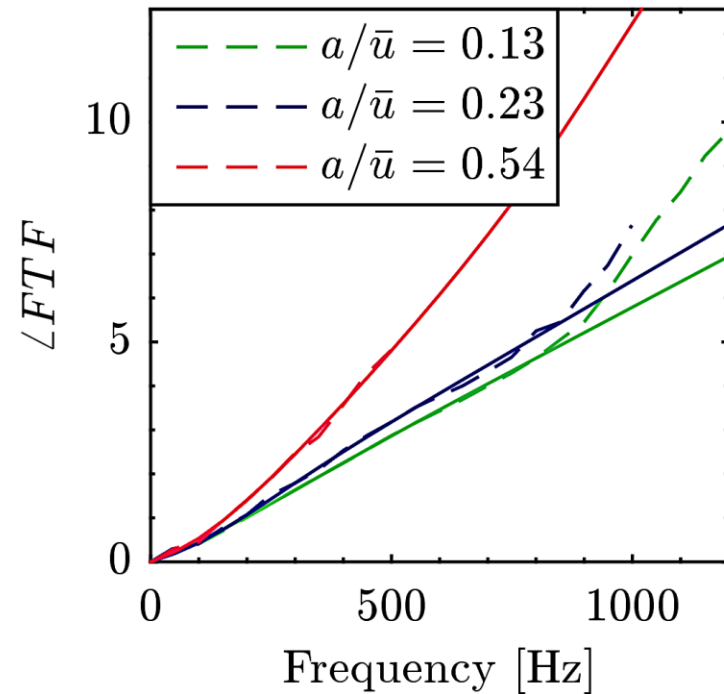
$\left. \begin{array}{l} \text{---} \text{---} \text{---} \\ \text{---} \text{---} \text{---} \\ \text{---} \text{---} \text{---} \end{array} \right\} \tilde{h}(\tau) \text{ (2 Gauss curves)}$

Results for $\mathcal{T}(\omega, a)$ and $\tilde{\mathcal{T}}(\omega, a)$

gain



phase



$\left. \begin{array}{l} \text{---} \\ \text{---} \\ \text{---} \end{array} \right\} \mathcal{T}(\omega, a)$

$\left. \begin{array}{l} \text{---} \\ \text{---} \\ \text{---} \end{array} \right\} \tilde{\mathcal{T}}(\omega, a) \text{ (2 Gauss curves)}$

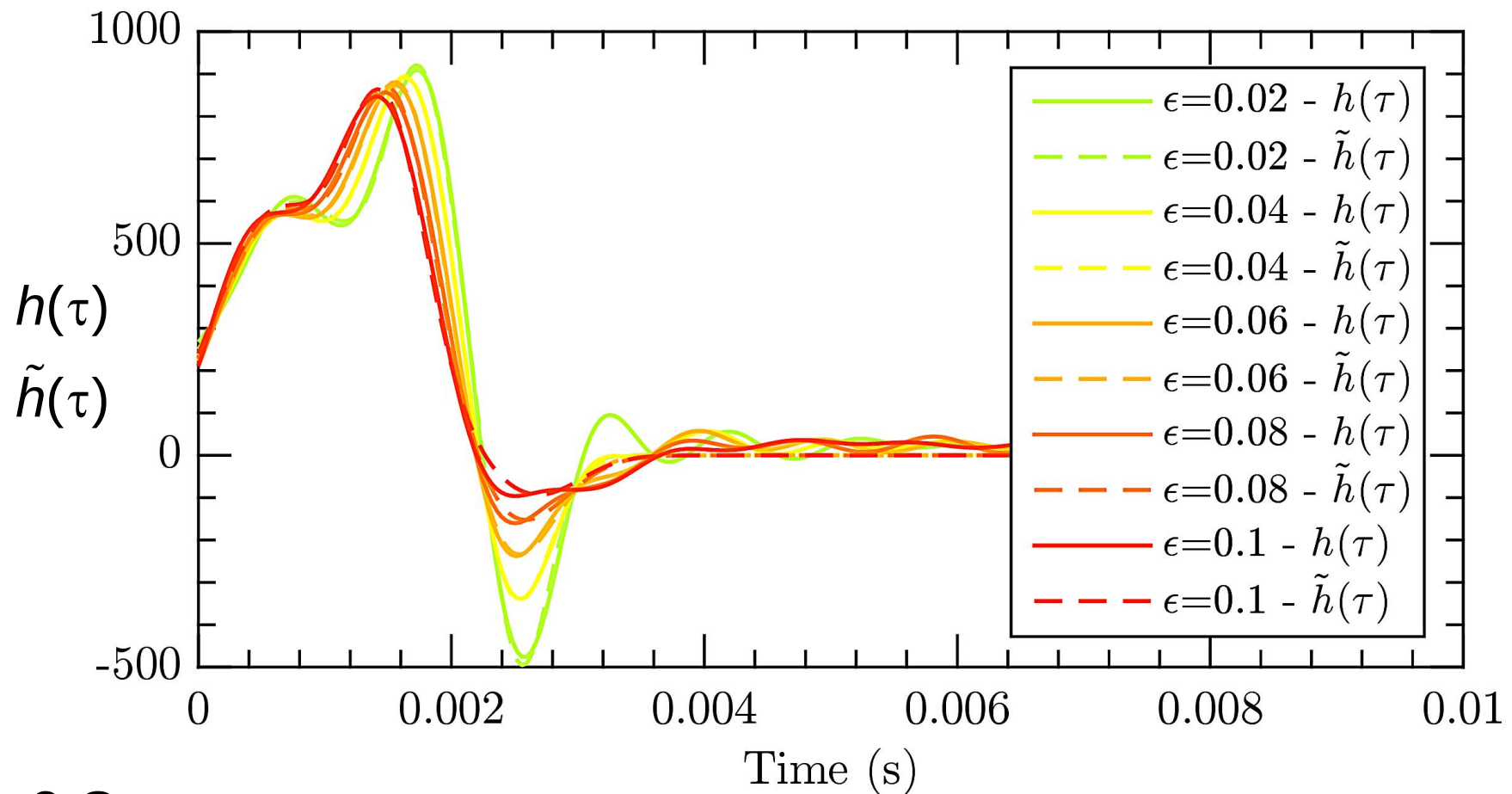
6.3. Application to CH₄ - H₂ flame

$\phi=0.95$

CH₄: 80%

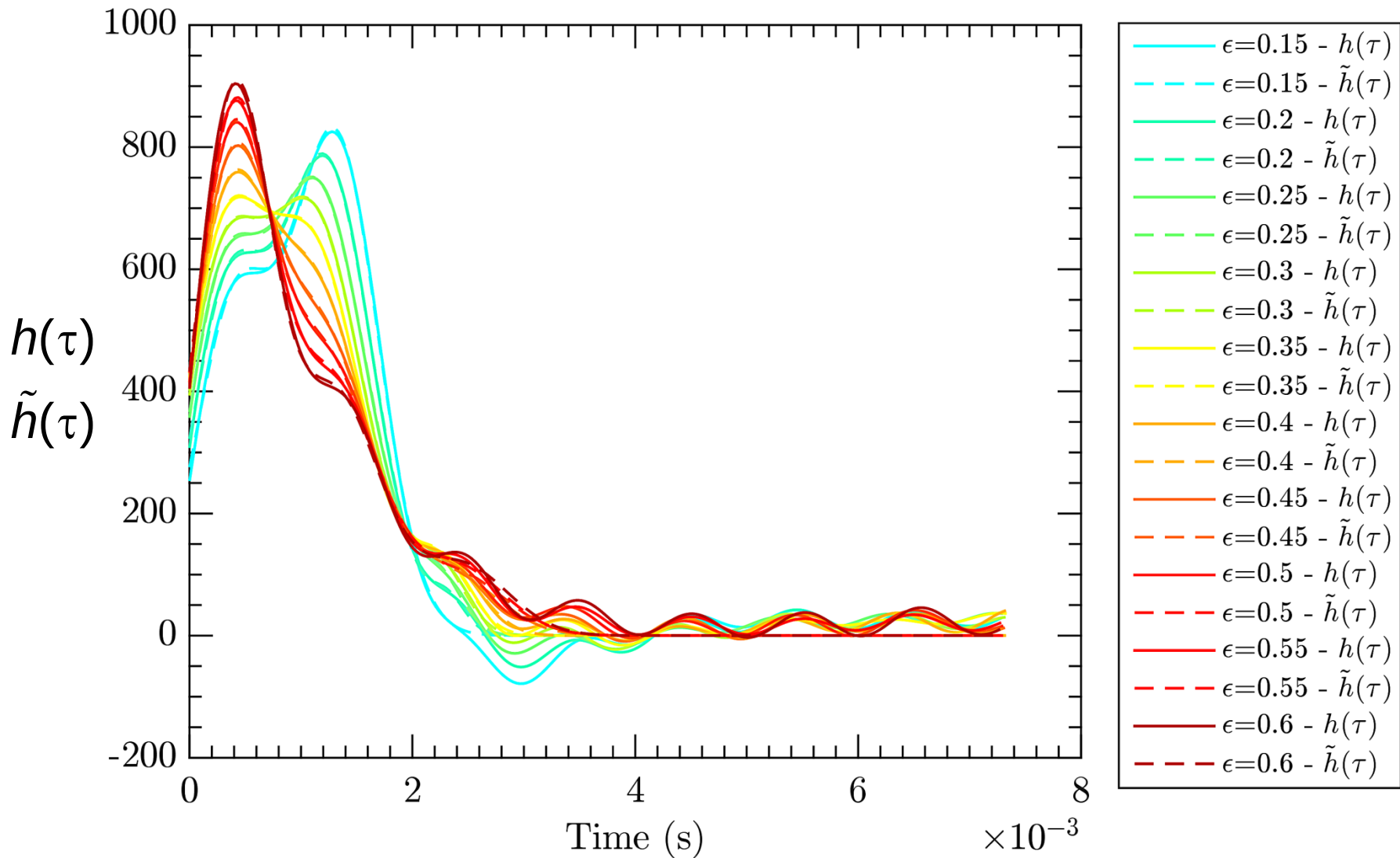
H₂: 20%

$\varepsilon = a / \bar{u}$



3 Gauss curves

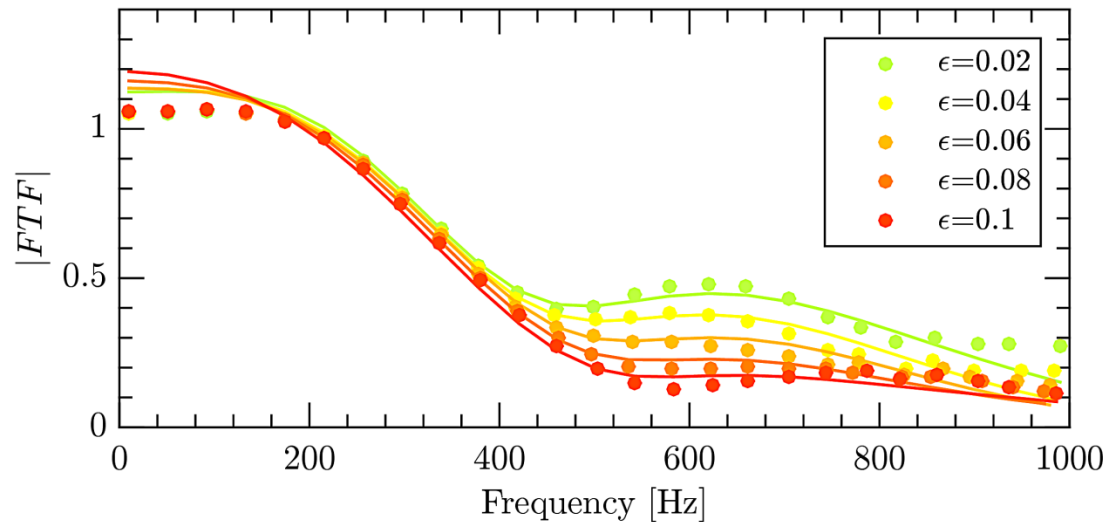
for higher amplitudes ($\epsilon = 0.15 \dots 0.6$):



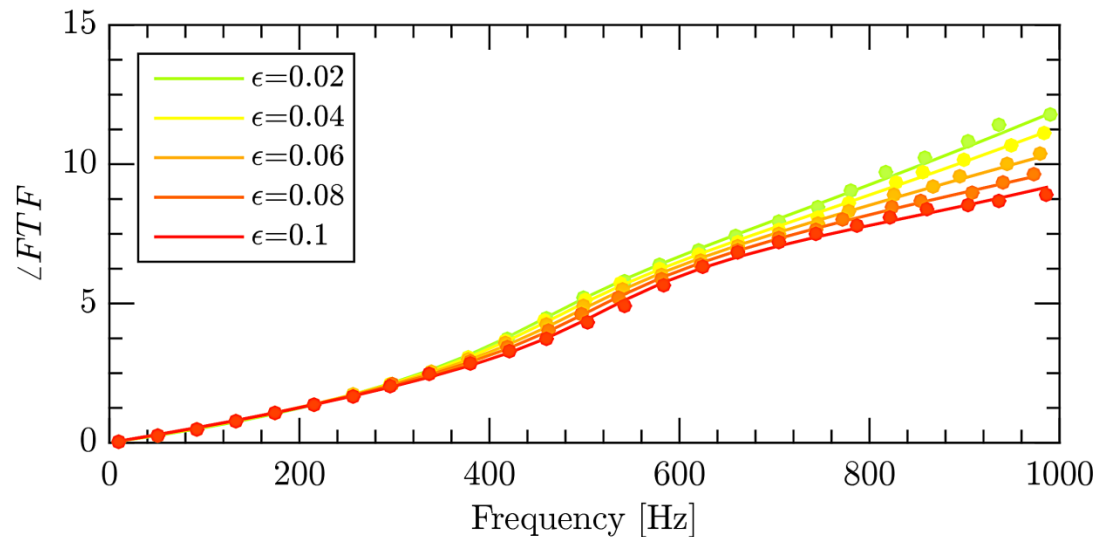
Results for $\mathcal{T}(\omega, a)$ and $\tilde{\mathcal{T}}(\omega, a)$

$$\varepsilon = a / \bar{u}$$

gain



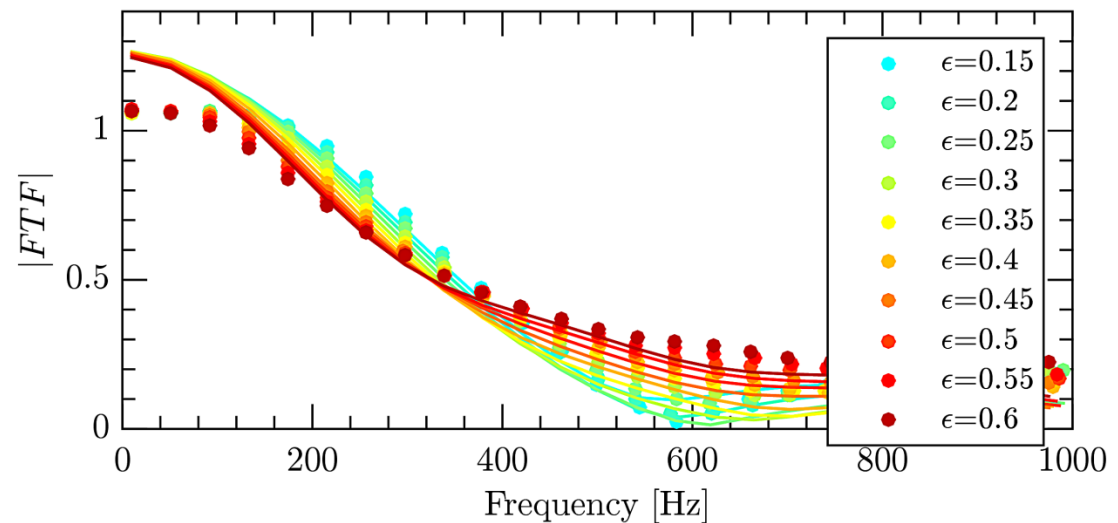
phase



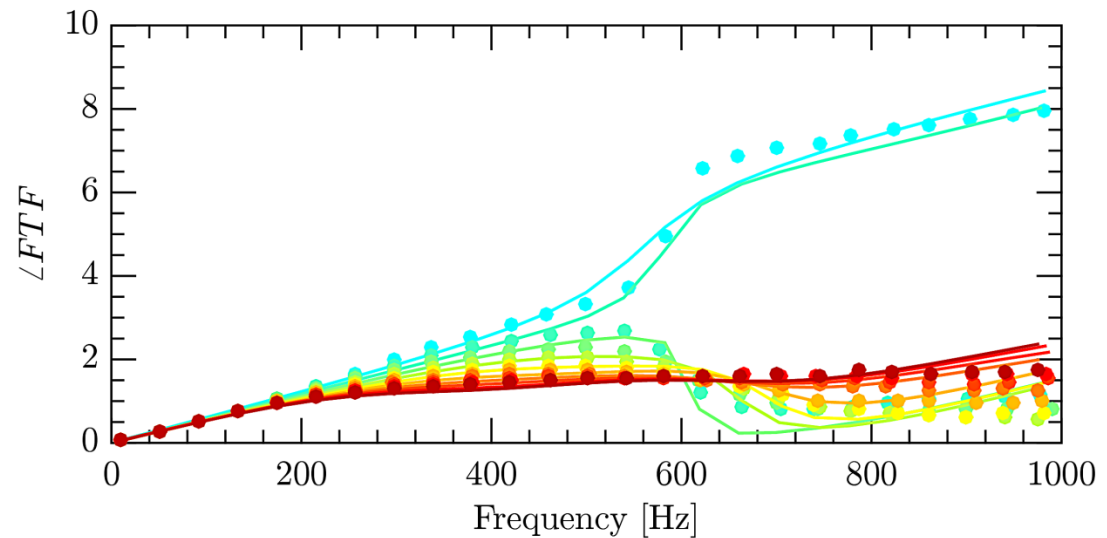
3 Gauss curves

for higher amplitudes ($\epsilon = 0.15 \dots 0.6$):

gain

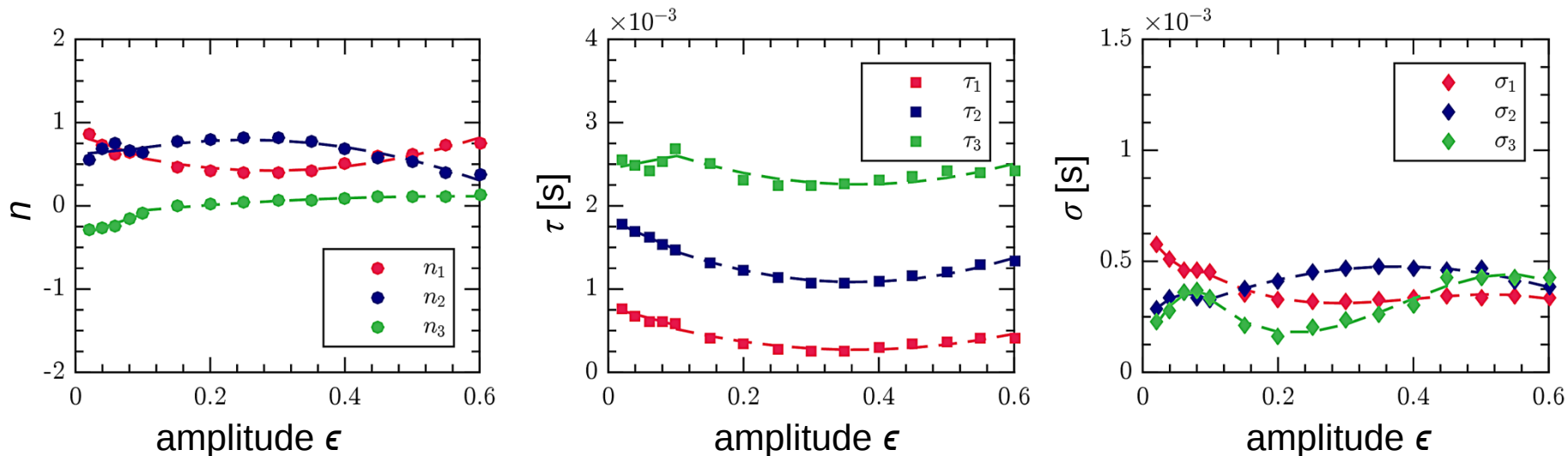


phase



3 Gauss curves

Amplitude-dependence of the fitting parameters



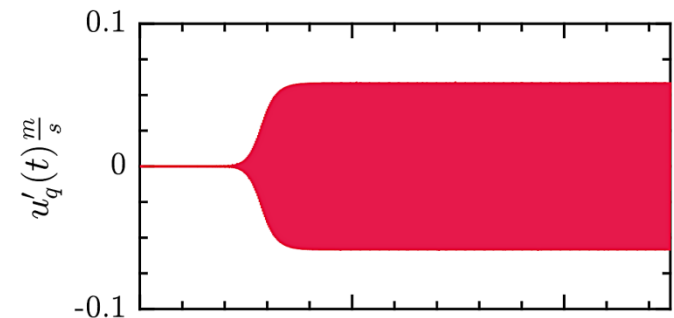
curve fitting with polynomials:

$$\left. \begin{aligned} n(a) &= n^{(0)} + n^{(1)}a + n^{(2)}a^2 + n^{(3)}a^3 + \dots \\ \tau(a) &= \tau^{(0)} + \tau^{(1)}a + \tau^{(2)}a^2 + \tau^{(3)}a^3 + \dots \\ \sigma(a) &= \sigma^{(0)} + \sigma^{(1)}a + \sigma^{(2)}a^2 + \sigma^{(3)}a^3 + \dots \end{aligned} \right\} \rightarrow \text{fully analytical time domain function } \tilde{h}(t, a)$$

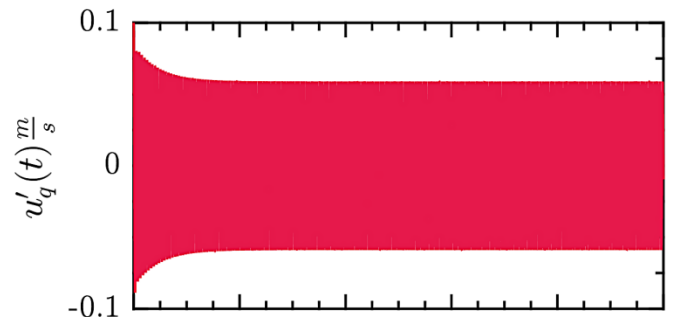
$\rightarrow$ fully analytical FDF, $\tilde{\mathcal{T}}(\omega, a)$

Time history predictions for CH₄ - H₂ flame in a $\lambda/4$ tube

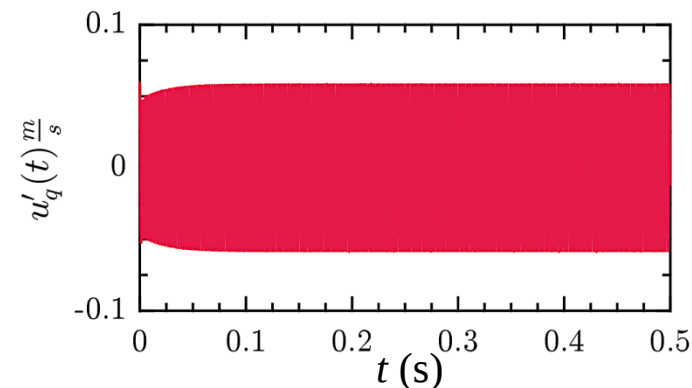
small initial
disturbance:



large initial
disturbance:



initial disturbance
similar to limit cycle
amplitude:



Gopinathan, S.M. and Heckl, Maria (2019) Stability analysis and flashback limits for combustion systems using hydrogen blends. *Proceedings of the 26th International Congress on Sound and Vibration*, 7-11 July 2019, Montreal, Canada, 8 pp.

7. Summary

- Description in frequency-domain by FTF, $\mathcal{T}(\omega)$
- Description in time-domain by impulse response, $h(\tau)$
- Analytical approximations $\tilde{\mathcal{T}}(\omega)$ and $\tilde{h}(\tau)$
- Same fitting parameters in frequency and time-domain
- Linear flame: fitting parameters are constant
- Nonlinear flame: fitting parameters depend on amplitude
 $h(\tau)$ is no longer an impulse response
- Amplitude-dependence can be described by simple functions
- Fully analytical description of flame

Thank you!

Maria Heckl and Sreenath M. Gopinathan
School of Chemical and Physical Sciences
Keele University
Staffordshire ST5 5BG
UK

m.a.heckl@keele.ac.uk
s.malamal.gopinathan@keele.ac.uk