Tubes with Internal Blockage: Evaluation of Stream functions and Eigen-Frequencies

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Overview of current work



Fig 1: Different flow regions in a tube with blockage

- The hydrodynamic region is treated as an acoustic lumped mass
- The physical blockage is replaced by a hypothetical Blockage Integral





1-D Mathematical model of tube with blockage



Fig 2: Schematic of a tube with area jump and blockage inside



1-D Mathematical model of tube with blockage



 \blacktriangleright At x=x₂

Figure same as previous slide

$$p_2(x,t) - p_3(x,t) = \rho_2 L_{eff} \left(\frac{\partial u_2(x,t)}{\partial t} \right)$$
$$u_2(x,t) = u_3(x,t)$$



1-D Mathematical model of tube with blockage

In matrix form we can write:

$$\begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 0 \\ e^{-jkx_1} & -e^{jkx_1} & -\overline{\rho c}\overline{S}e^{-jkx_1} & \overline{\rho c}\overline{S}e^{jkx_1} & 0 & 0 \\ e^{-jkx_1} & e^{jkx_1} & -e^{jkx_1} & -e^{jkx_1} & 0 & 0 \\ 0 & 0 & e^{-jkx_2} & -e^{jkx_2} & -\overline{\rho c}e^{-jkx_2} & \overline{\rho c}e^{jkx_2} \\ 0 & 0 & (1-jL_{eff}\omega/c)e^{-jkx_2} & (1+jL_{eff}\omega/c)e^{jkx_2} & -e^{-jkx_2} & -e^{jkx_2} \\ 0 & 0 & 0 & 0 & e^{-jkL} & e^{jkL} \end{bmatrix} \begin{bmatrix} A_1 \\ B_1 \\ A_2 \\ B_2 \\ A_3 \\ B_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Made use of Newton-Raphson method to solve the characteristic equation



Concept of Blockage Integral: Effective value of blockage



Blockage Integral,

$$L_{eff} = \int_0^L ((1/r) \,\partial \Psi / \partial r) \,d\xi - L$$





Concept of Blockage Integral



Fig 4: Modified combustor model with blockage lying on a single hypothetical plane





Streamline Generation



Fig 5: Streamlines for tube with high blockage



Pressure profile in presence of blockage (for Mode 1)



Fig 6: Pressure profile for blockage location, x=0.25L



Modal frequency variation with respect to tube parameters

- Objective is to find out how modal frequency changes with respect to
- 1. Blockage inside tube (expressed by blockage integral)
- 2. Area jump within the tube
- 3. Temperature jump within the tube



Section 1: Effect of blockage on modal frequency

> Assumptions:

- 1. Effect of Area Jump neglected
- 2. Effect of Thermal Jump neglected



Section 1: Effect of blockage on modal frequency



Fig 9: Blockage location, x=0.25L



Section 1: Analysis using pressure profile (for Mode 1)



Effect of Blockage Integral on Modal Frequency

• Reason for this response:

$$p_1 - p_2 = \rho L_{eff} \left(\frac{\partial u}{\partial t} \right)$$

- > When particle velocity=0, blockage does not have any effect
- When particle velocity is maximum, blockage has maximum effect





Section 2: Effect of temperature jump on modal frequency

Assumption:

- 1. The Thermal Jump is step jump and not gradual
- 2. Effect of Area Jump neglected
- 3. Effect of blockage has been included in analysis.



Section 2: Effect of temperature jump on modal frequency



Fig 13: Temperature jump location, x=0.25L



Section 2: Analysis using pressure profile (for Mode 1)





• Assumptions:

- 1. Effect of blockage is neglected
- 2. Thermal jump is neglected
- 3. Area Jump is step jump and not gradual













Fig 20: pressure profile describing impact of area jump on modal frequency



Section 3: Analysis using pressure profile (for Mode 1)





Section 3: Analysis using pressure profile (for Mode 1)







Special case: Analysis for combined area jump and blockage



Fig 23: Tube with combined area jump and blockage at the same location

Hard to write the pressure continuity equation at area expansion

$$p_1 - p_2 = \rho L_{eff} \left(\partial u / \partial t \right)$$



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Special case: Analysis for combined area jump and blockage



By adding two pressure jump equations,

$$p_1 - p_3 = j\rho\omega \left(L_{eff\,1}u_1 + L_{eff\,2}u_2\right)$$



Result Verification: Use of Perturbation Method

$$\succ f = f_n + \varepsilon$$

- \blacktriangleright In other notation, $\omega = \omega_n + 2\pi\varepsilon$
- → Characteristic equation, $f(\omega) = 0$, leads to
- $\succ f(\omega_n + 2\pi\varepsilon) = 0$

In the final form,
$$\varepsilon = f(L_{eff}, (S_2/S_1), (c_1/c_2), (\rho_1/\rho_2))$$

or, we can say, $\omega = f(L_{eff}, (S_2/S_1), (c_1/c_2), (\rho_1/\rho_2))$





Result Verification: for variable blockage value



Fig 24: Blockage location, x=0.25L





Result Verification: for variable area jump



Fig 25: Area jump location, x=0.25L



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Result Verification: for variable temperature jump



Fig 26: Temperature jump location, x=0.25L



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Conclusions made so far

- 1. Modal frequency decreases as blockage integral increases
- 2. Modal frequency may increase/decrease w.r.t area jump
- 3. Modal frequency increases w.r.t. thermal jump





Scope of Future Work

- Cross check of the results for the case when blockage and area jump location coincide
- Identify the effect of mean flow in analysis
- Try to verify these models through simulations/experimental works





Thank you

