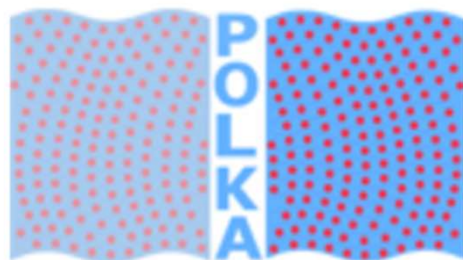


POLKA 6th Scientific Workshop:
Identifying key features from noisy time
traces: instabilities, bifurcations and
intermittency



Claire Bourquard

March 16th, 2023

Montestigliano



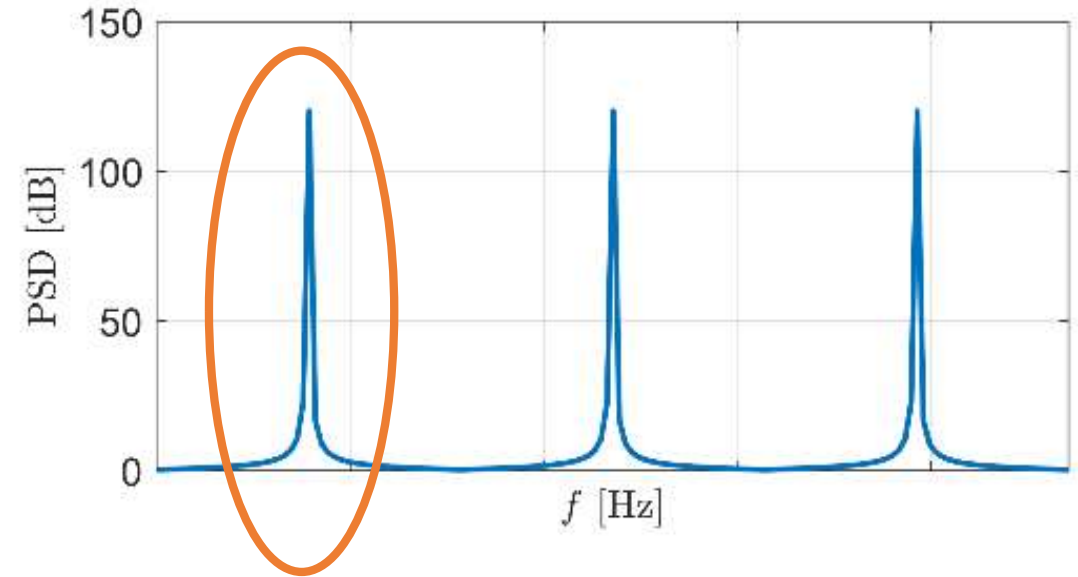
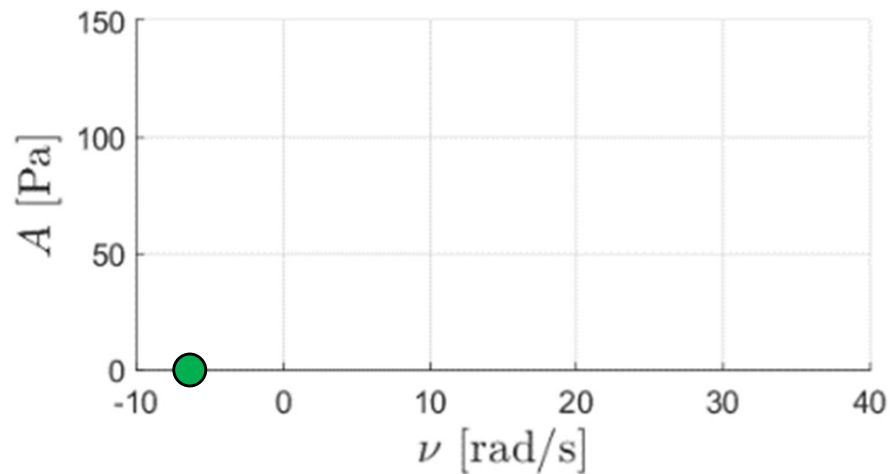
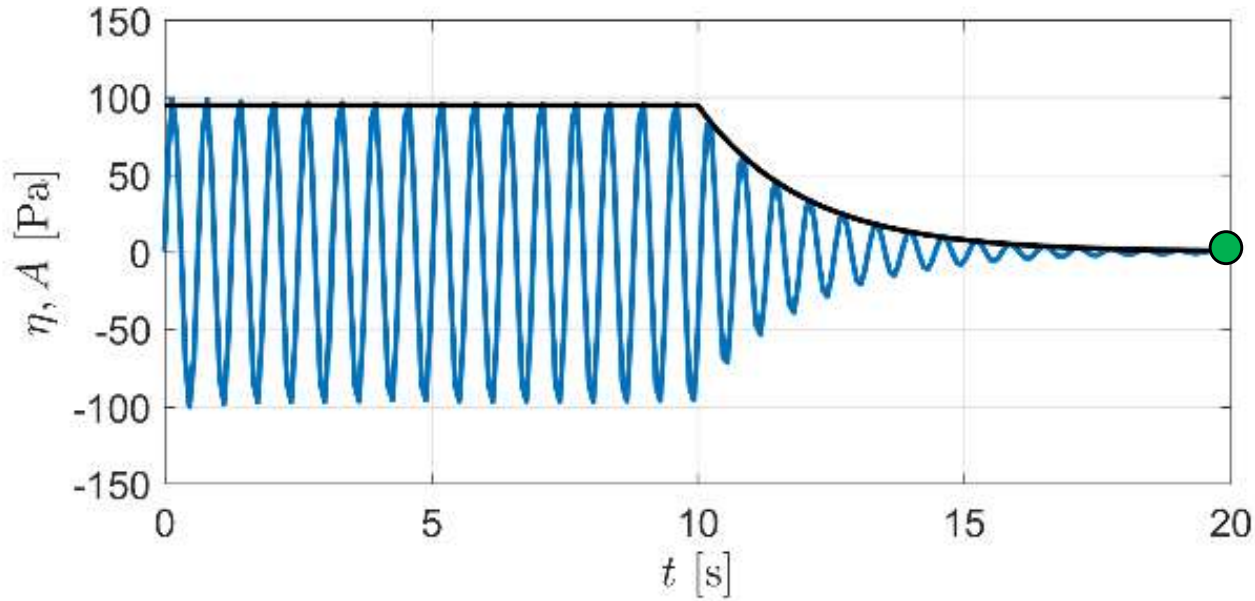
ETH zürich

Agenda

- Basics of stochastic nonlinear dynamics
- Back to your experimental system: how to characterize it?
- Low order modeling

Basics of stochastic nonlinear system dynamics

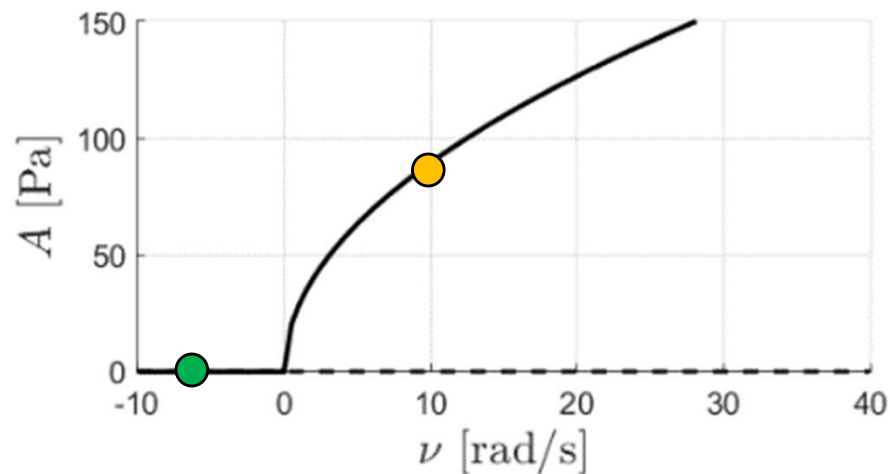
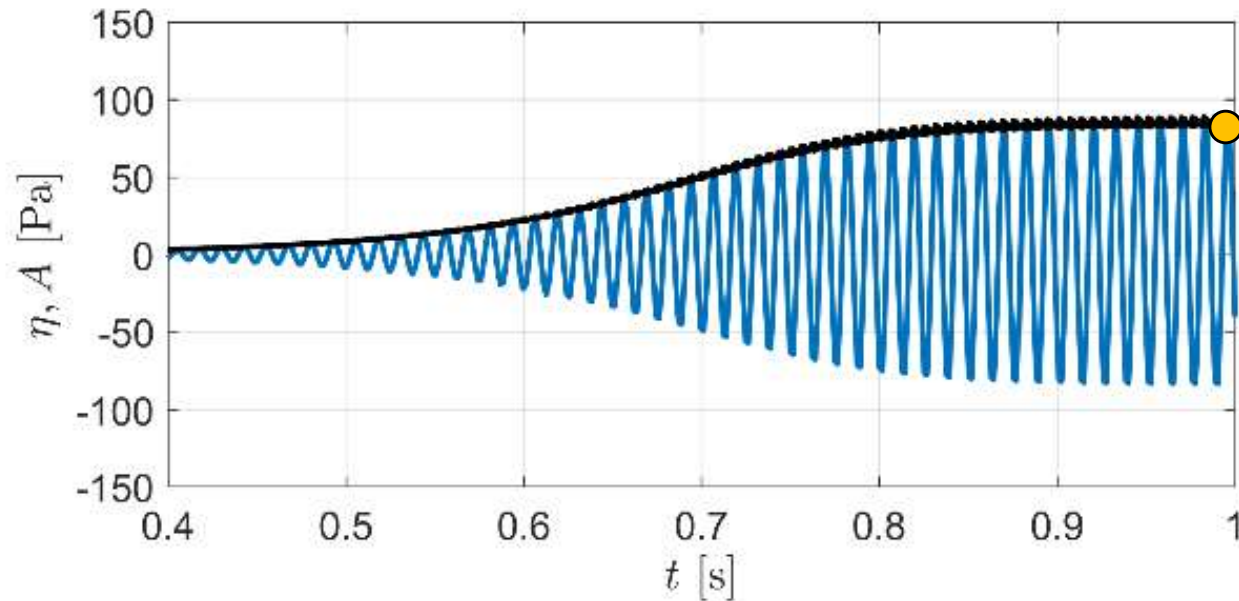
Deterministic dynamics: stable point



$$\ddot{\eta} - 2\nu\dot{\eta} + \omega_0^2\eta = F \sin(\omega_f t)$$

$$\nu = -7 \text{ rad/s}$$

Deterministic dynamics: Hopf bifurcation (supercritical)



- Linearly unstable mode $\nu = 10 \text{ rad/s}$
- With saturation

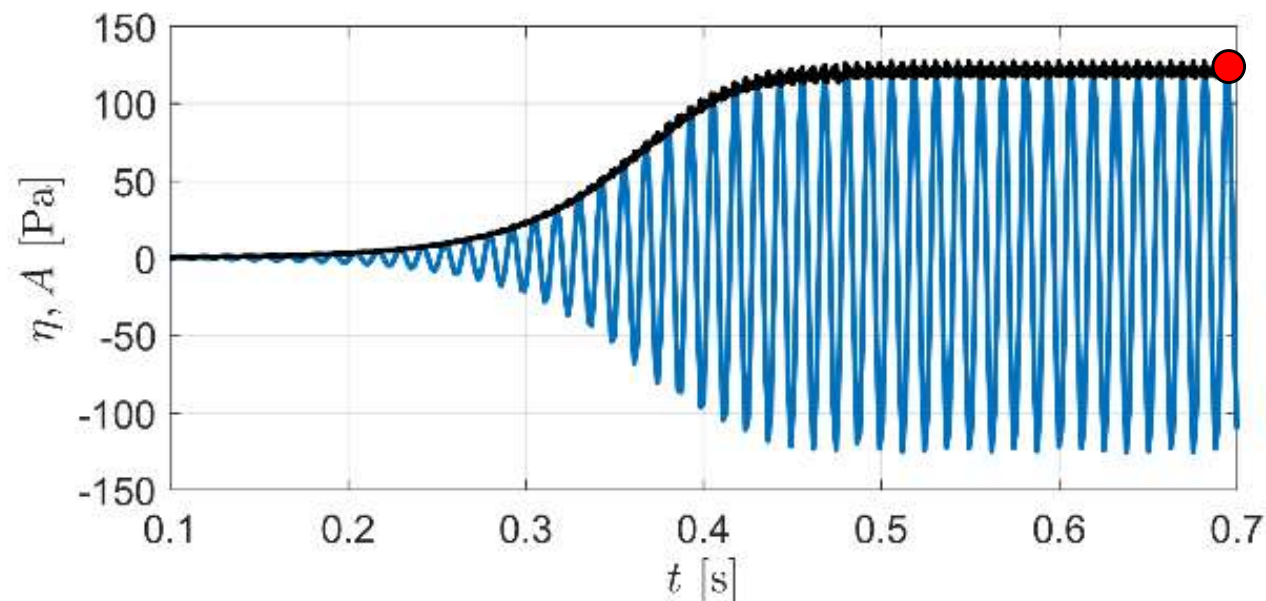
$$\ddot{\eta} - (2\nu + \kappa\eta^2)\dot{\eta} + \omega_0^2\eta = 0$$

Van der Pol equation

$$\eta = A \cos(\omega t)$$

$$A = \sqrt{-\frac{8\nu}{\kappa}}$$

Deterministic dynamics: Hopf bifurcation (supercritical)



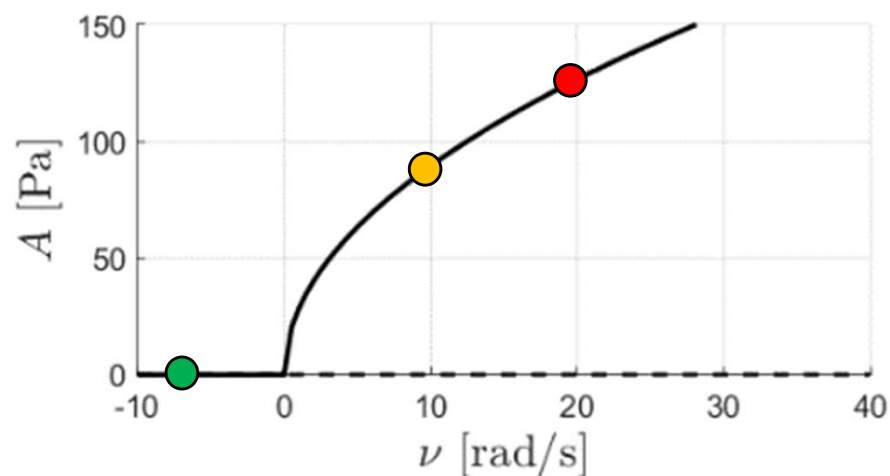
- Linearly unstable mode $\nu = 20$ rad/s
- With saturation

$$\ddot{\eta} - (2\nu + \kappa\eta^2)\dot{\eta} + \omega_0^2\eta = 0$$

Van der Pol equation

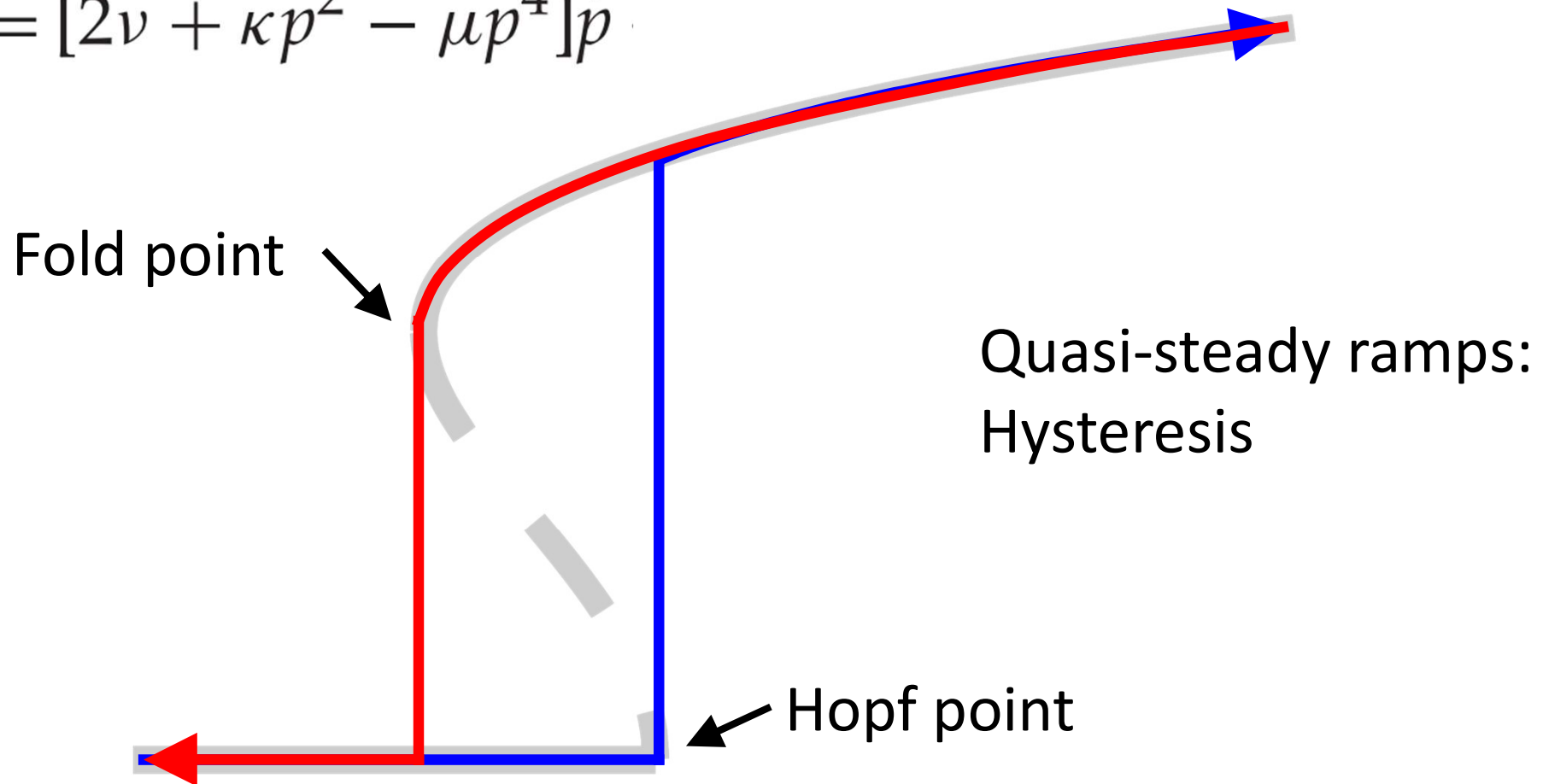
$$\eta = A \cos(\omega t)$$

$$A = \sqrt{-\frac{8\nu}{\kappa}}$$



Deterministic dynamics: subcritical bifurcation

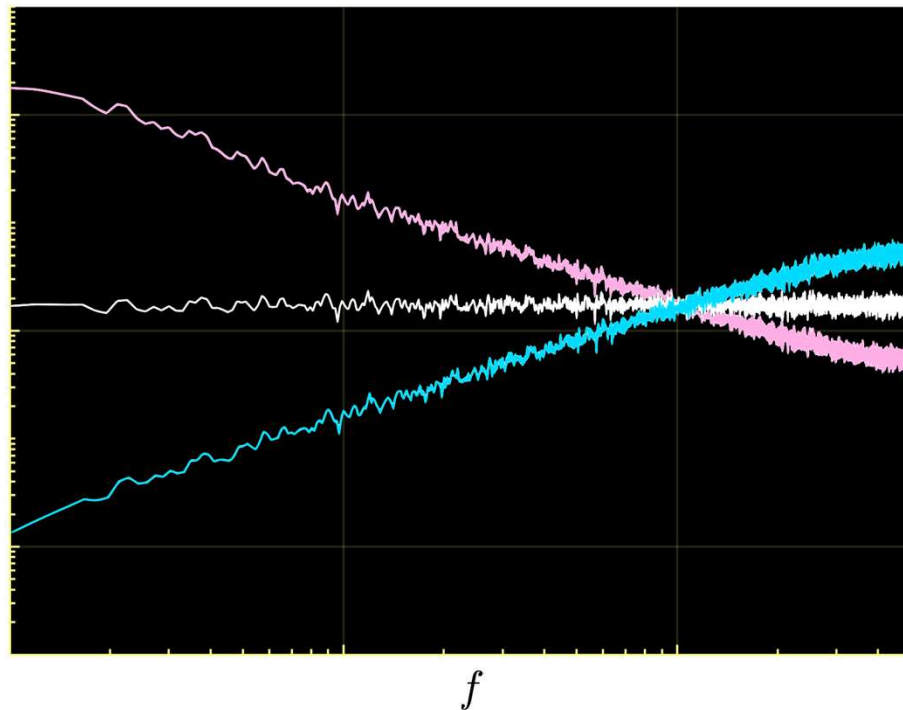
$$\ddot{p} + \omega_0^2 p = [2\nu + \kappa p^2 - \mu p^4] \dot{p}$$



Courtesy of G. Bonciolini

Stochastic dynamics: white vs. colored noise

Noise color \leftrightarrow Spectral content



Pink Noise
-3 dB/oct.



White Noise
constant

OK



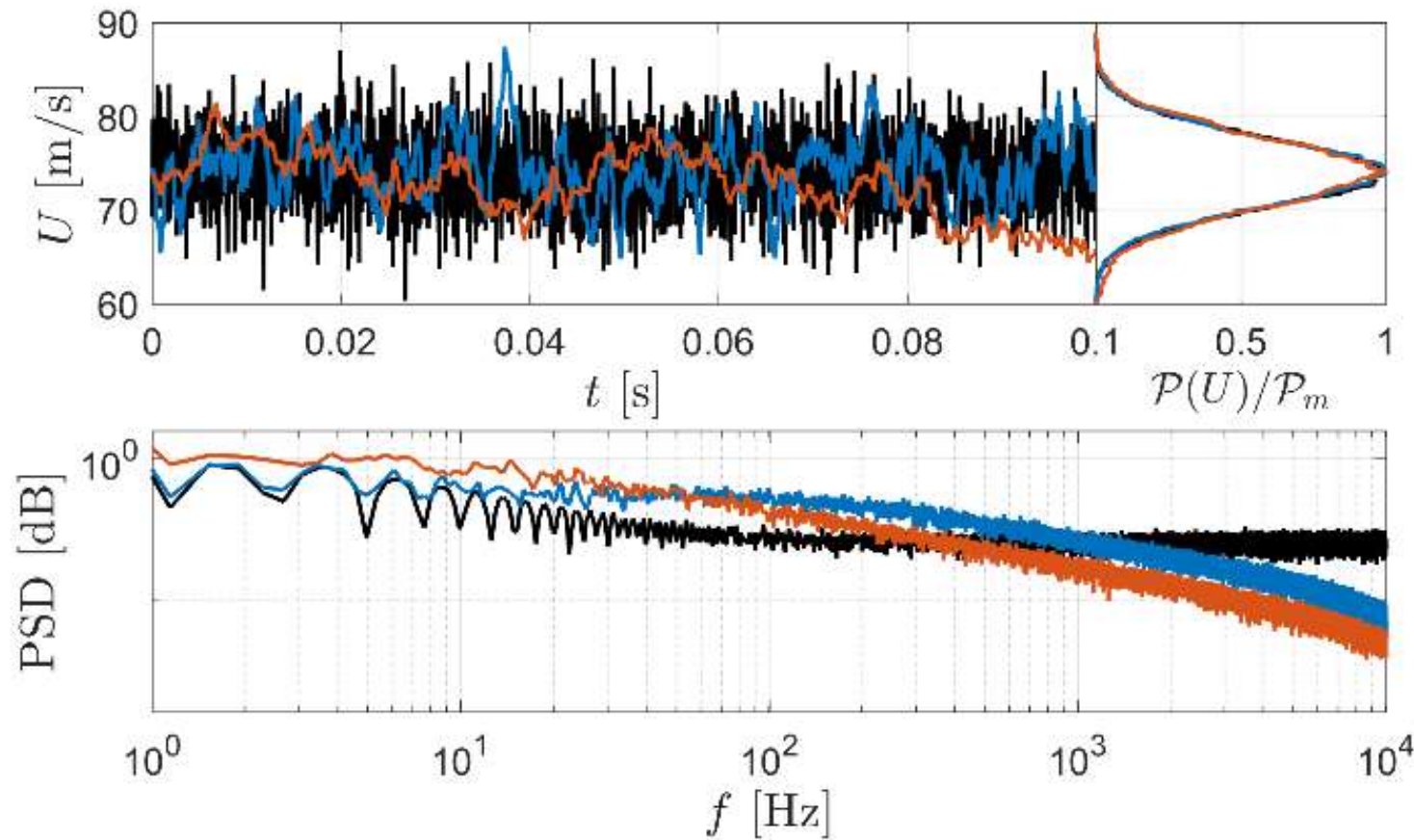
Blue Noise
+3 dB/oct.

Bonciolini, Boujo, Noiray, "Output-only parameter identification of a colored-noise-driven Van-der-Pol oscillator: Thermoacoustic instabilities as an example", Physical Review E, (2017).

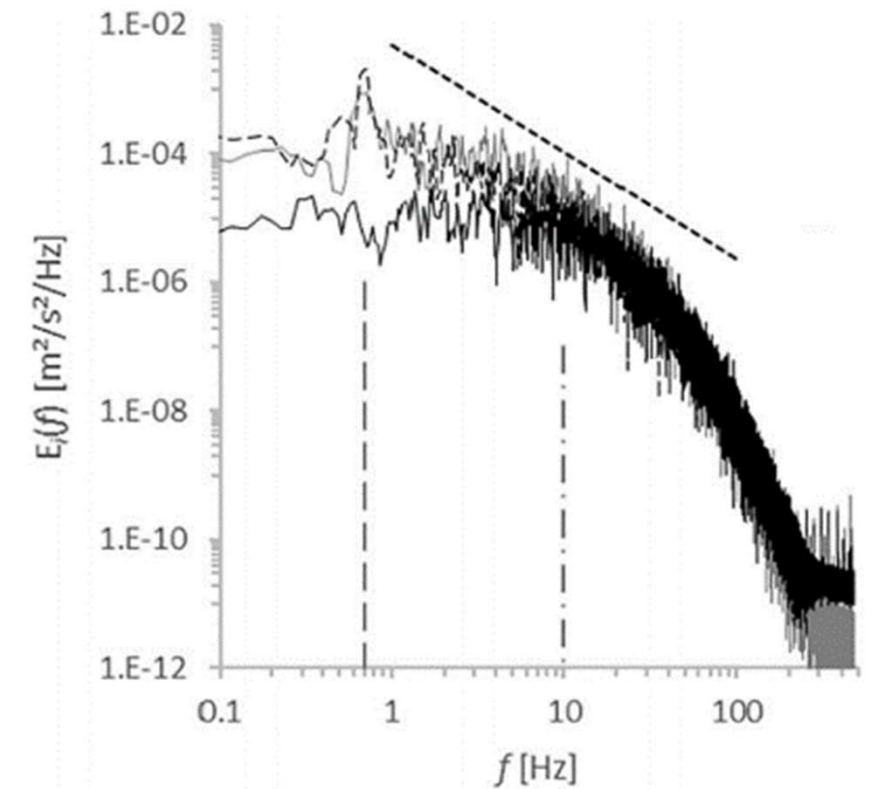
Courtesy of G. Bonciolini

Stochastic dynamics: white vs. colored noise

$$U = \bar{U}(1 + \chi(t))$$



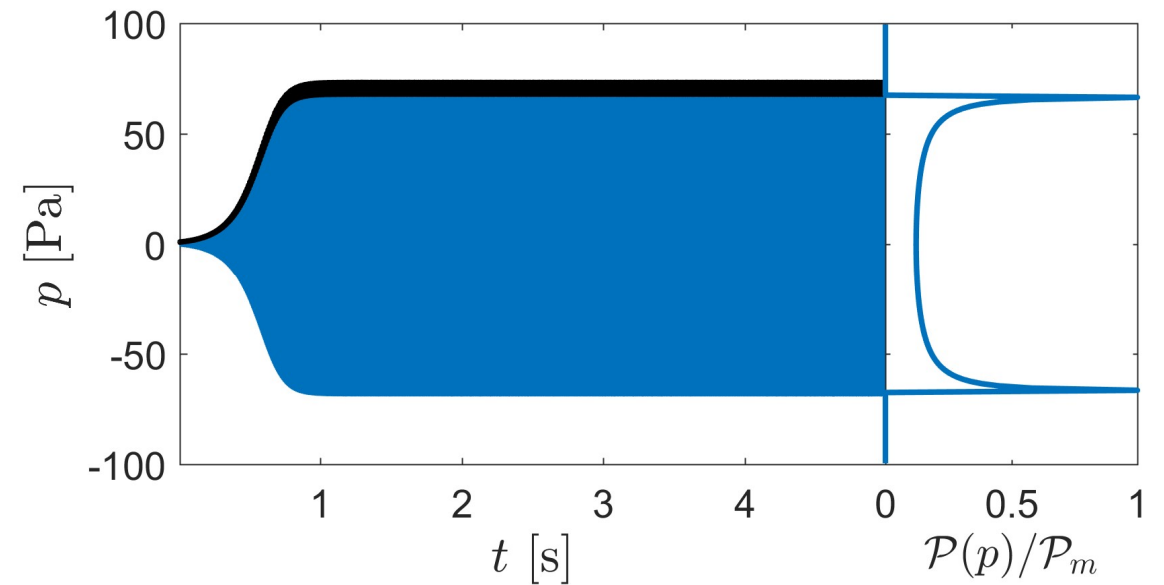
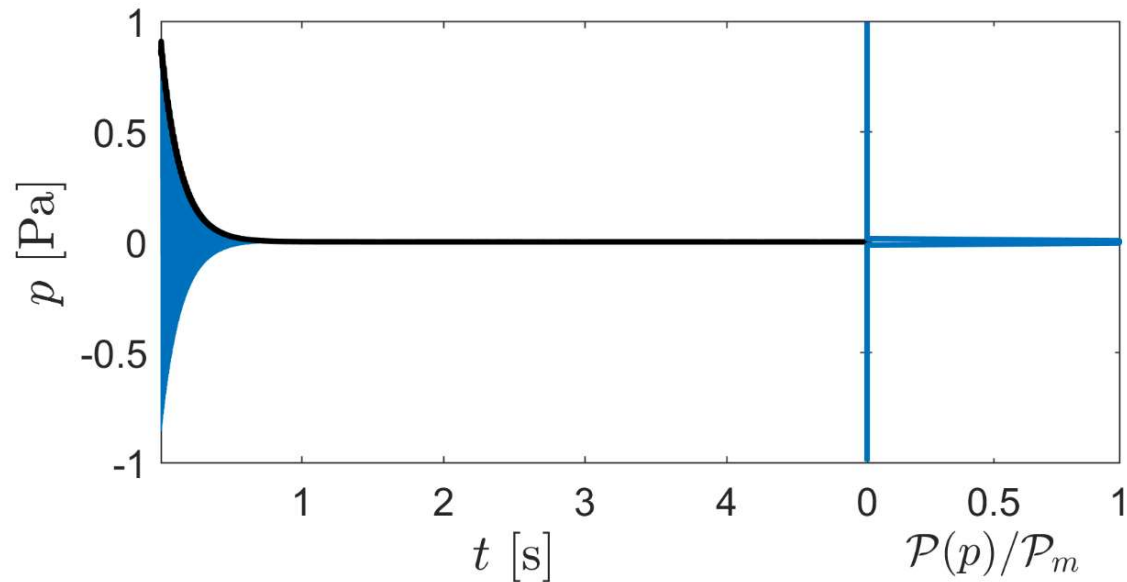
$$\dot{\chi} = -\frac{\chi}{\tau} + \zeta_{\chi}$$



From Giacomelli et al., 2020

Stochastic dynamics: typical probability density function

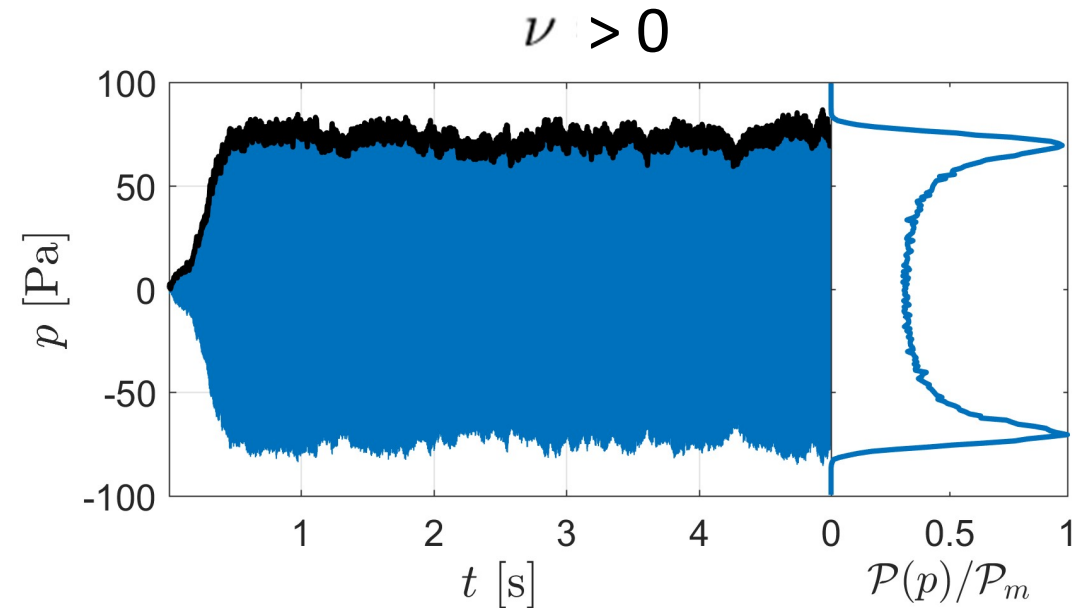
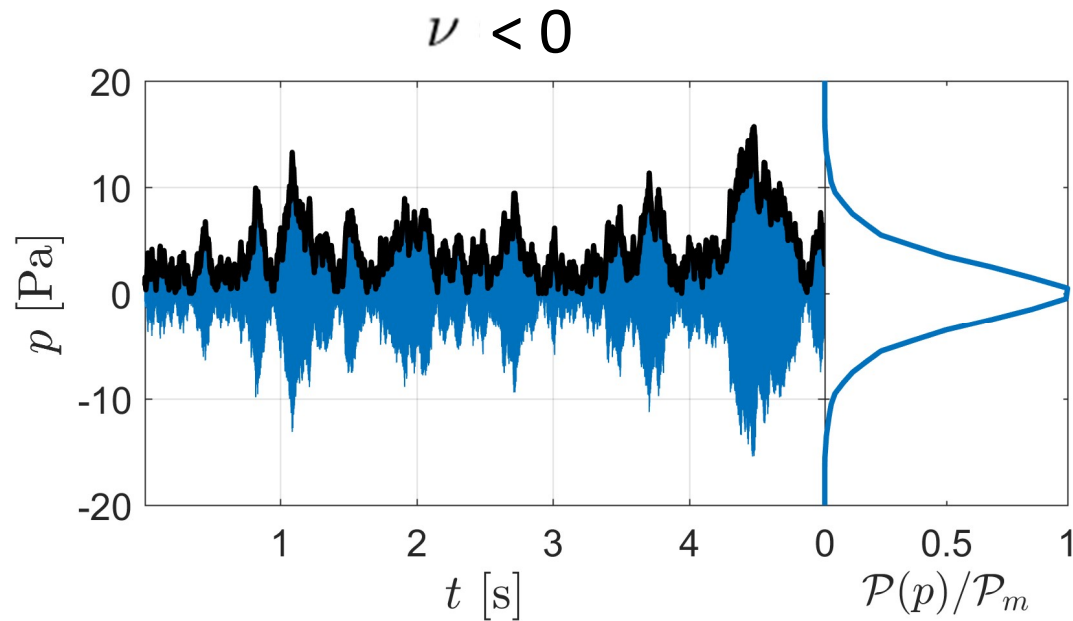
Deterministic pressure PDFs: stable vs. unstable



Stochastic dynamics: typical probability density function

Addition of noise:

$$\ddot{\eta} + (-2\nu + \kappa\eta^2) \dot{\eta} + \omega_0^2 \eta = \xi(t)$$



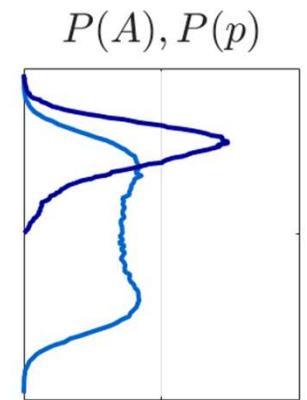
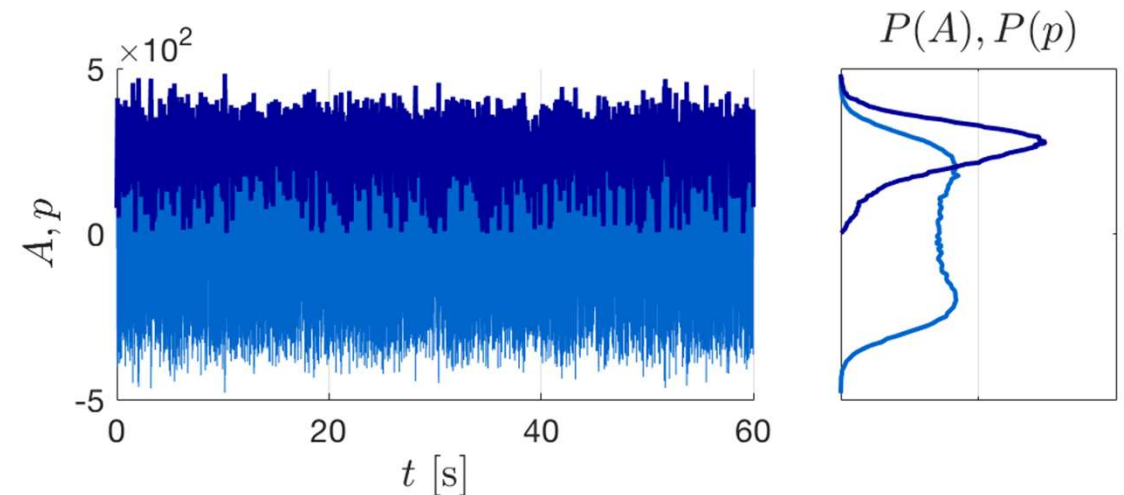
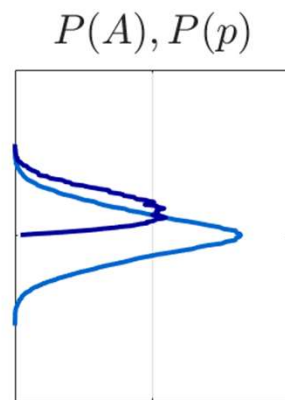
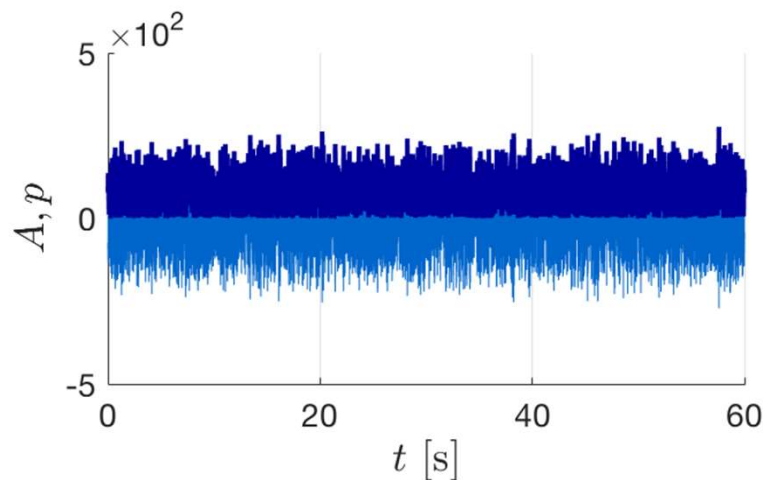
Stochastic dynamics: typical probability density function

Amplitude PDFs:

$$\ddot{\eta} + (-2\nu + \kappa\eta^2) \dot{\eta} + \omega_0^2 \eta = \xi(t)$$

$\nu < 0$

$\nu > 0$



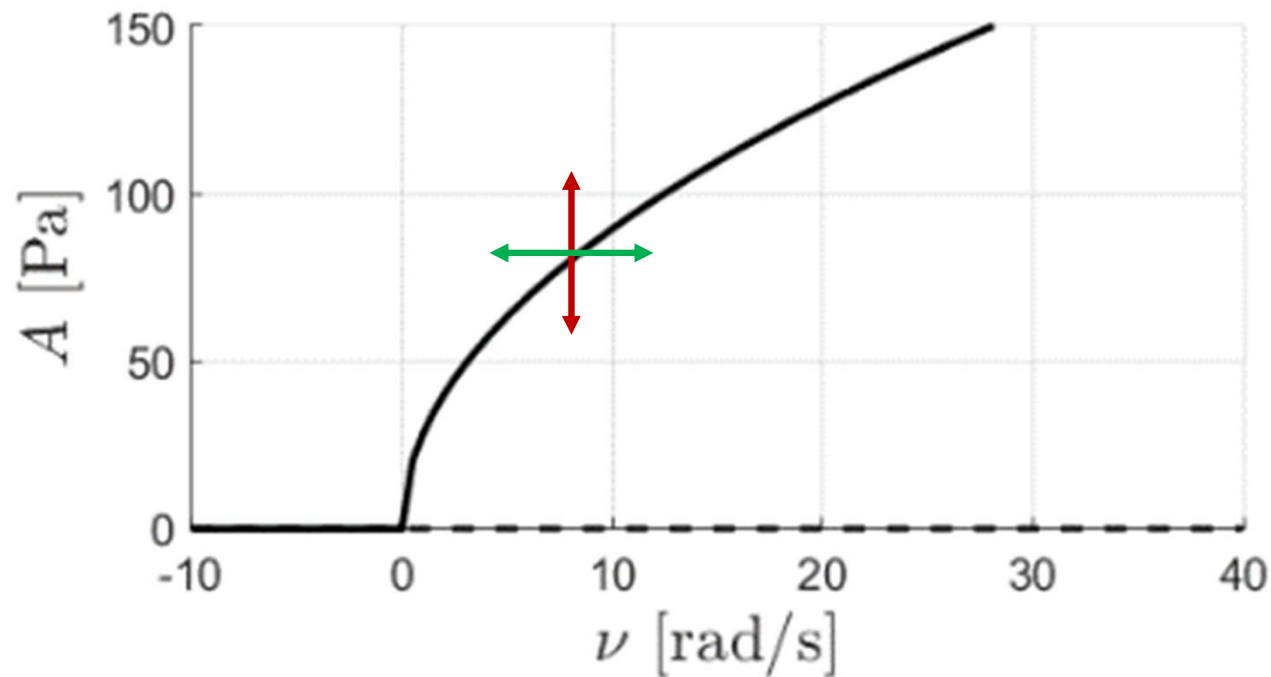
Stable
Resonance

vs.
vs.

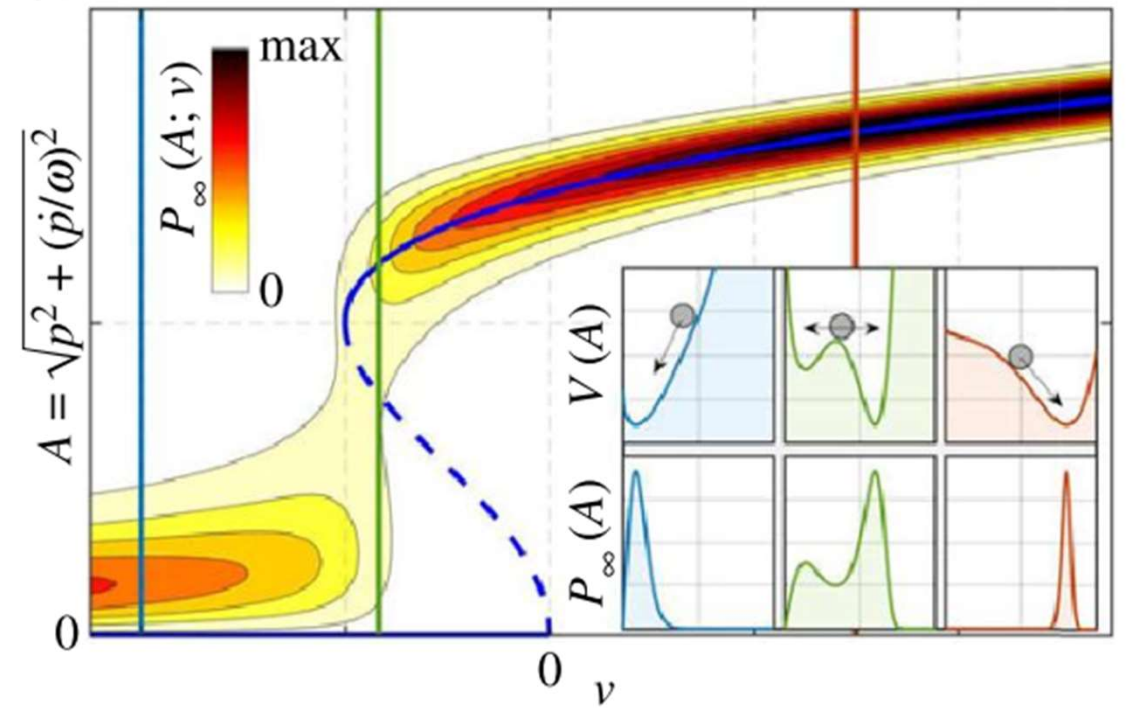
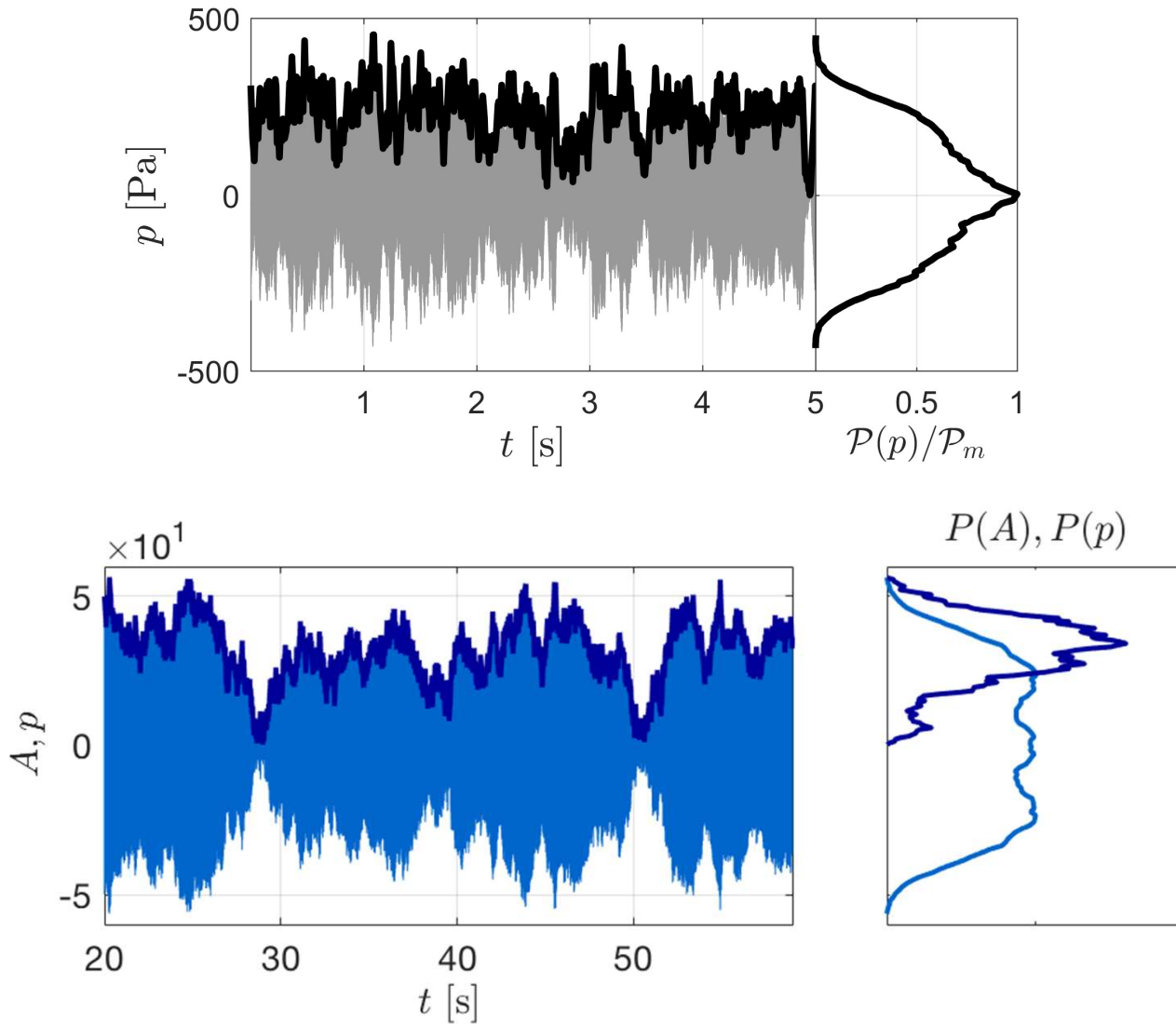
Unstable system
Instability

Stochastic dynamics: additive vs. multiplicative noise

$$\ddot{\eta} + (-2[\bar{\nu} + \chi(t)] + \kappa\eta^2) \dot{\eta} + \omega_0^2 \eta = \xi(t)$$



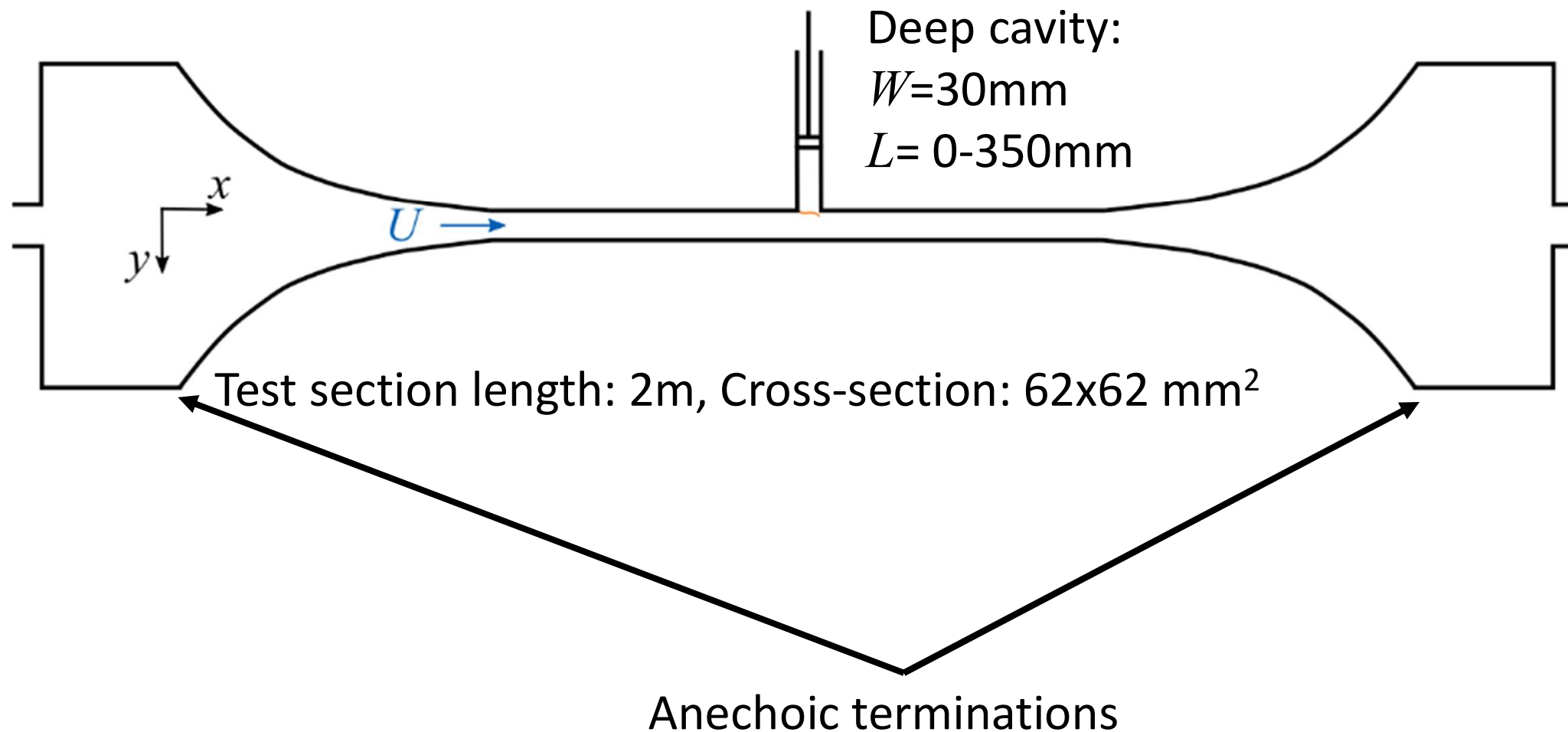
Intermittency: PDFs evidence:



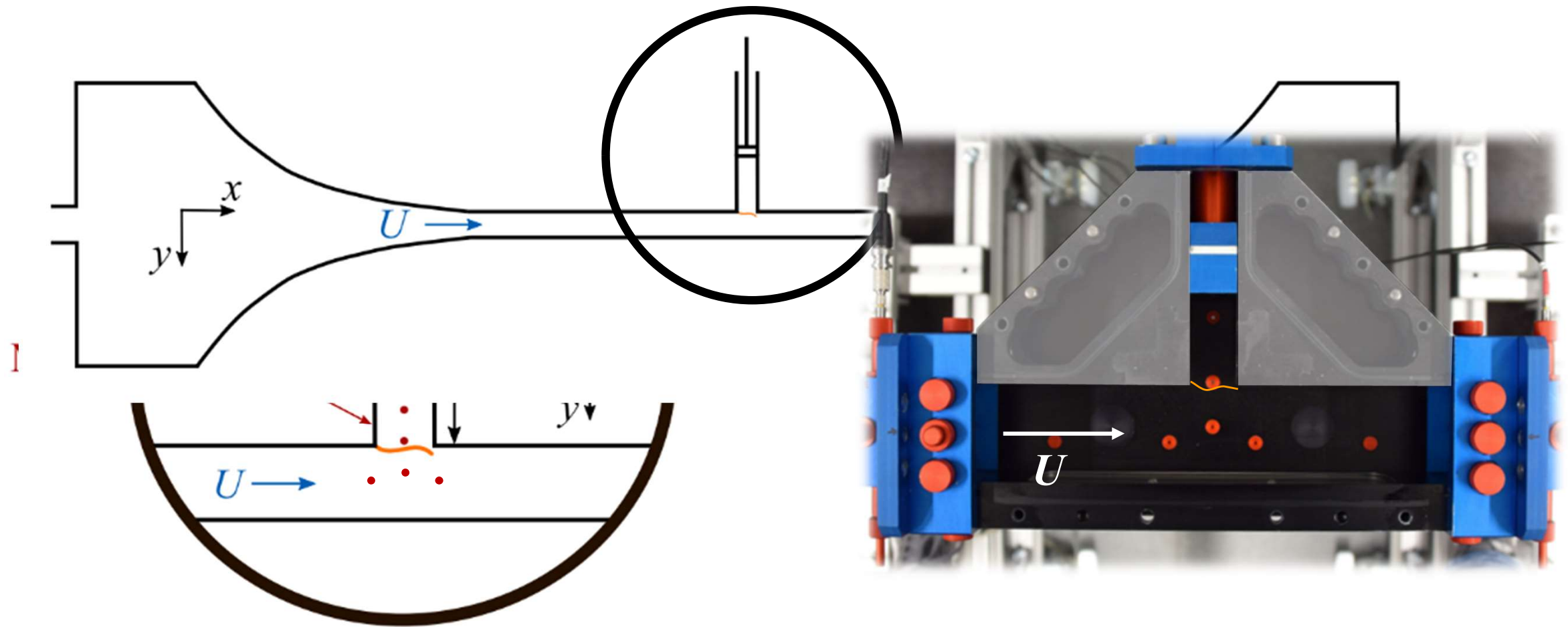
Courtesy of G. Bonciolini

Characterizing your experimental system

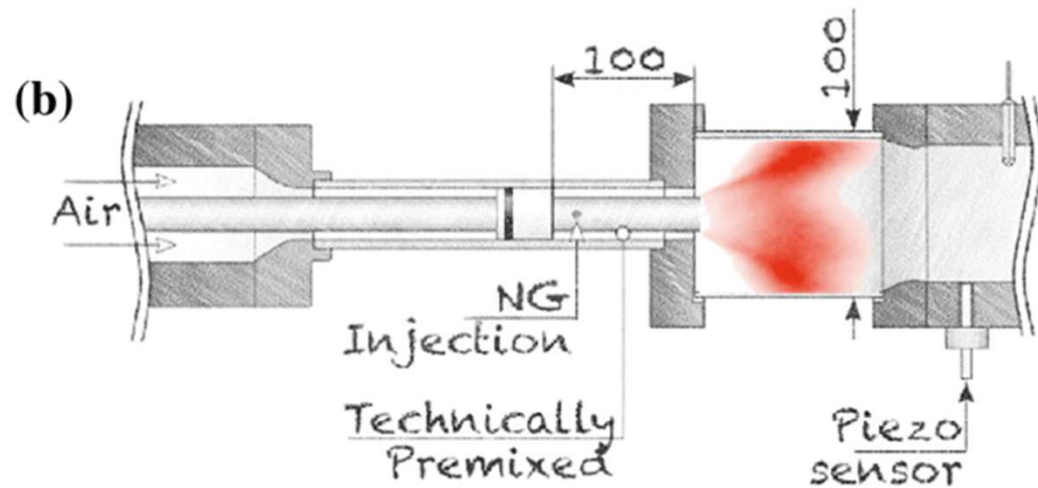
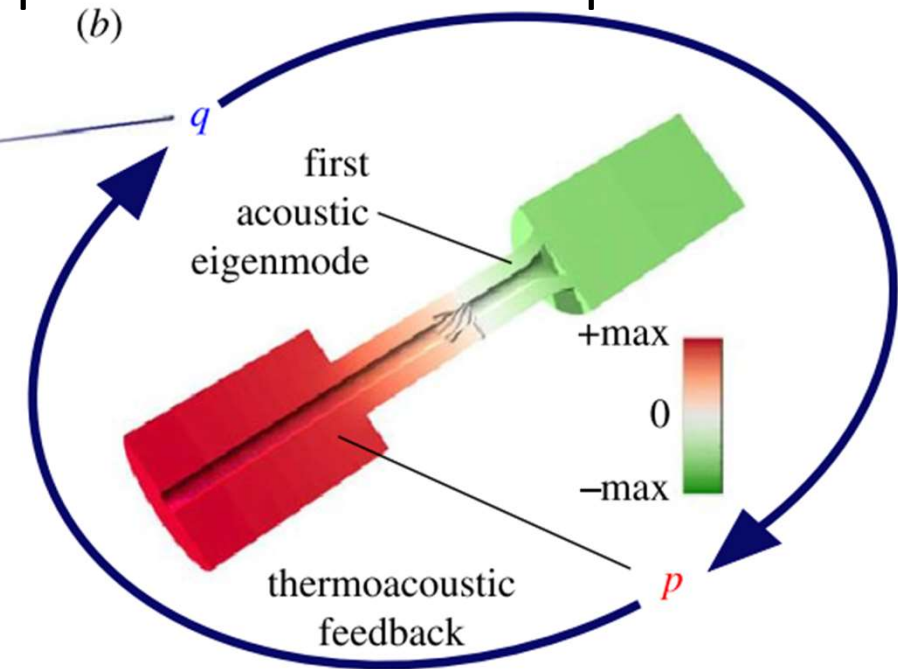
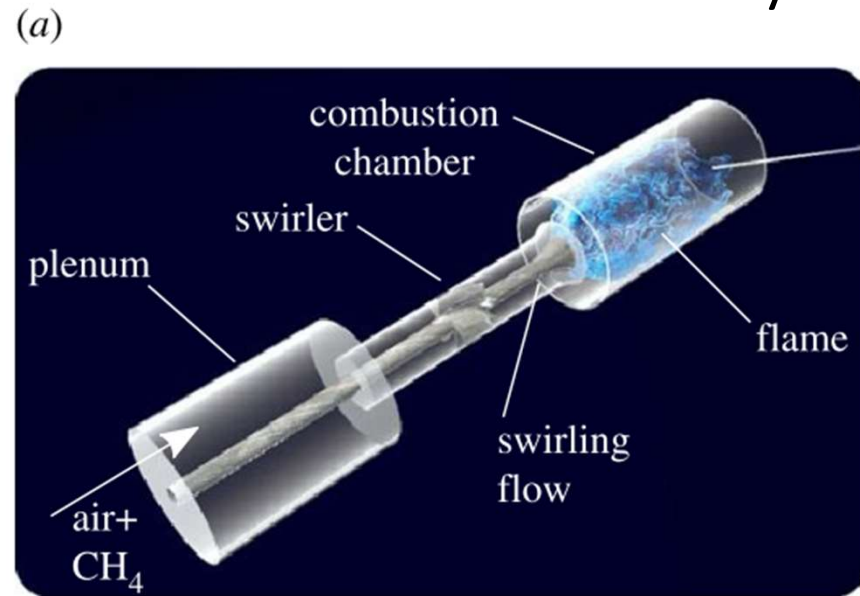
Introducing an aeroacoustic instability: experimental setup



Introducing an aeroacoustic instability: experimental setup



Introducing a thermoacoustic instability: experimental setup



Courtesy of G. Bonciolini

How to characterize your experimental setup?

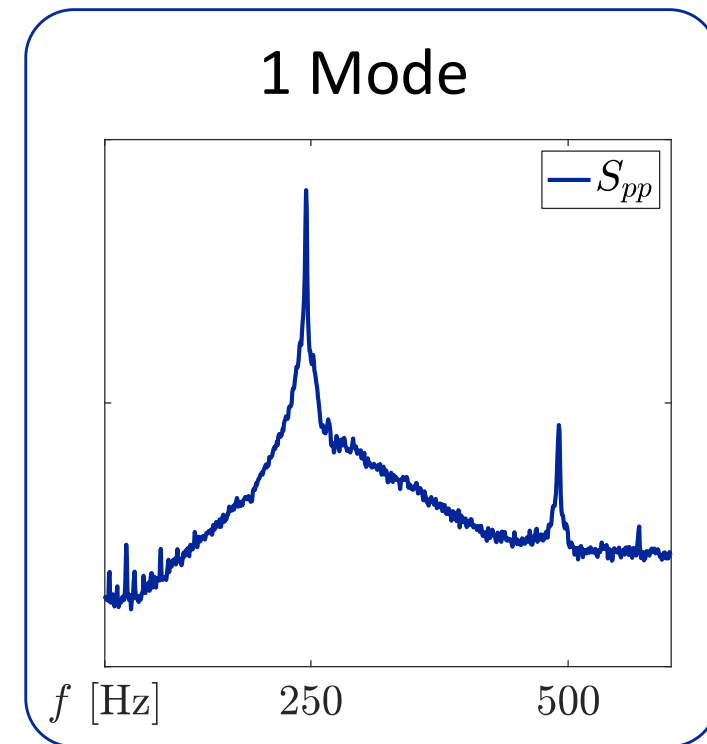
- Need for a scalar measure of amplitude:
 - Microphone time trace
 - Photomultiplier sensor
 - Average of unsteady velocity field in certain area...

Spectrum analysis: choose your mode!

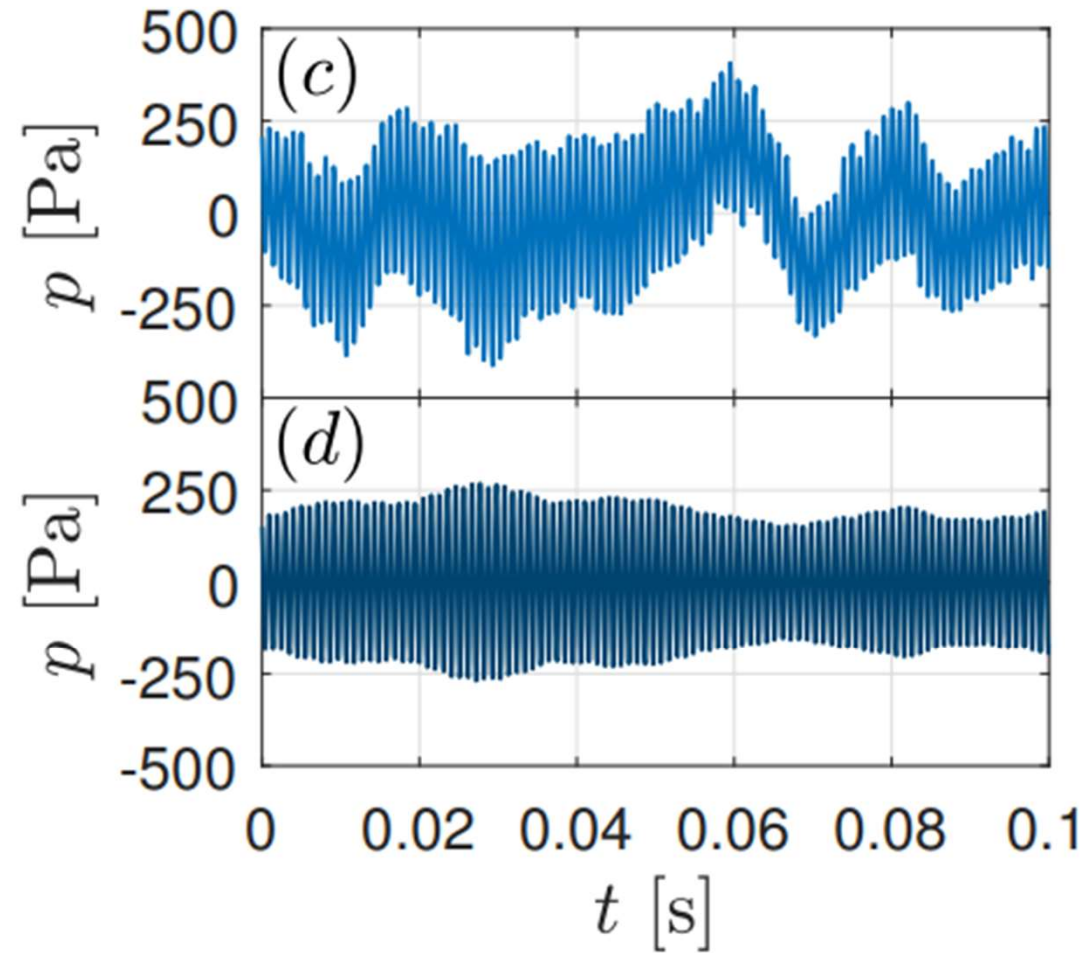
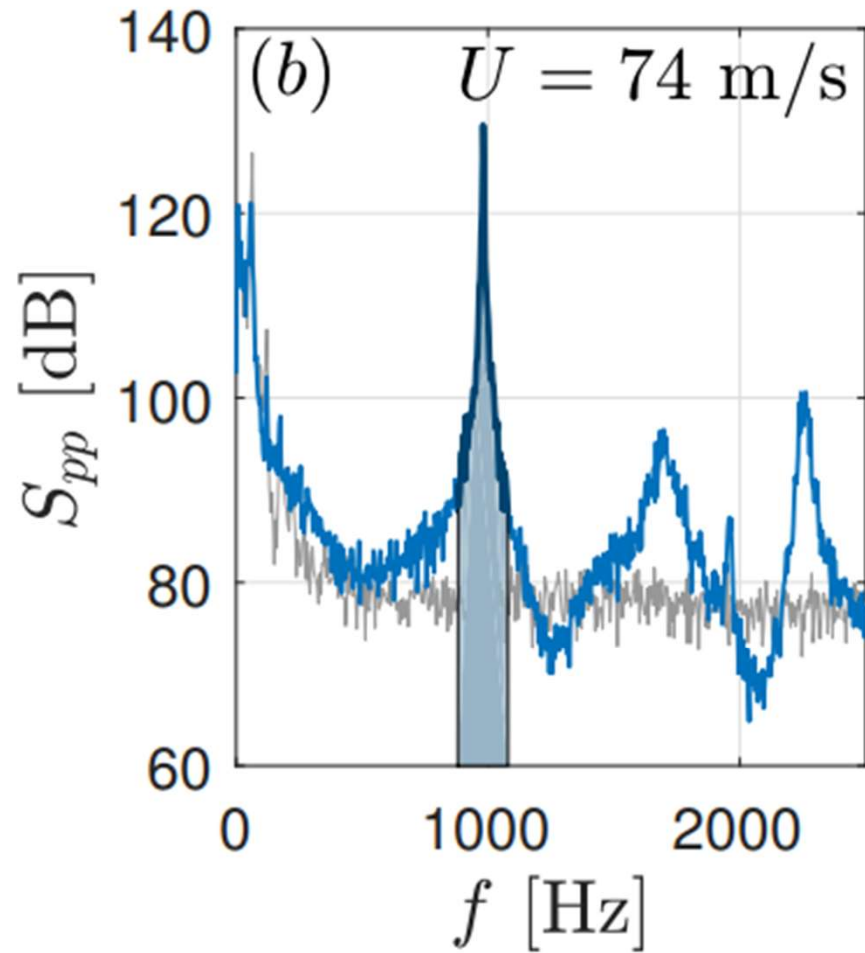
$$p(\mathbf{x}, t) = \sum_{i=1}^{\textcircled{N}} \psi_i(\mathbf{x}) \eta_i(t)$$

$$\ddot{\eta}_i + \omega_i^2 \eta_i = 2\nu_i \dot{\eta}_i - g_i(\eta_j, \dot{\eta}_j) + \xi_i$$

Experiment – 2 Modes



The importance of filtering:



Do's and don'ts

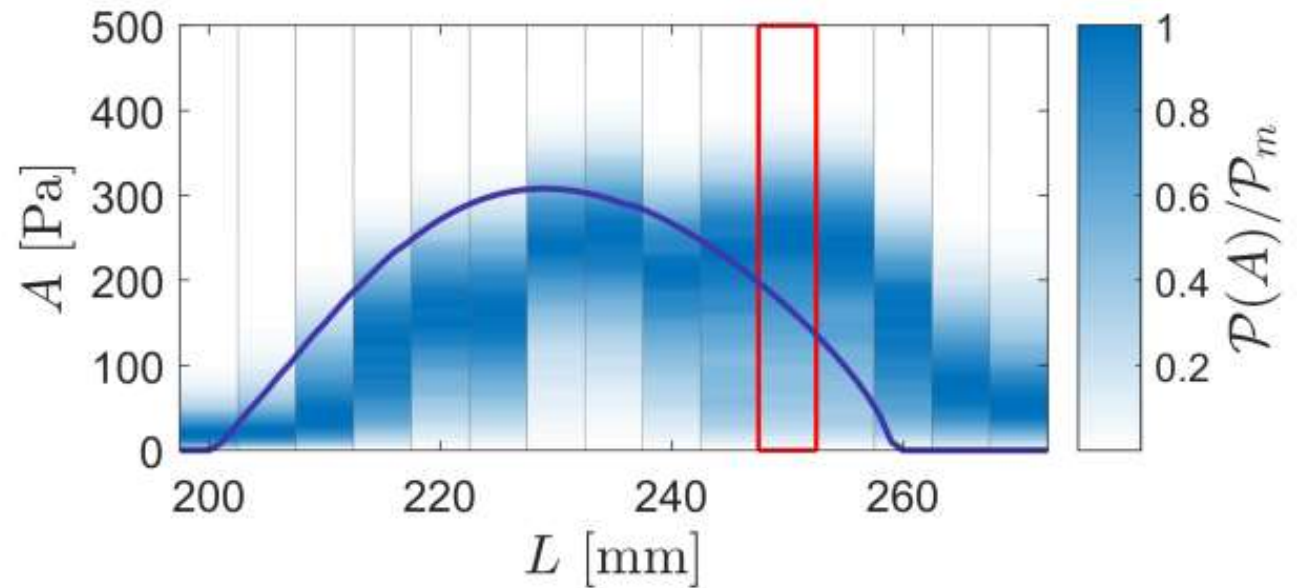
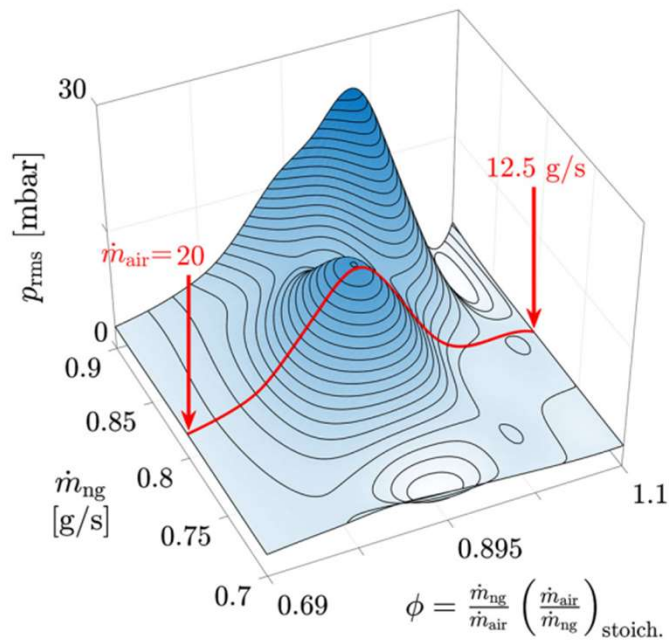
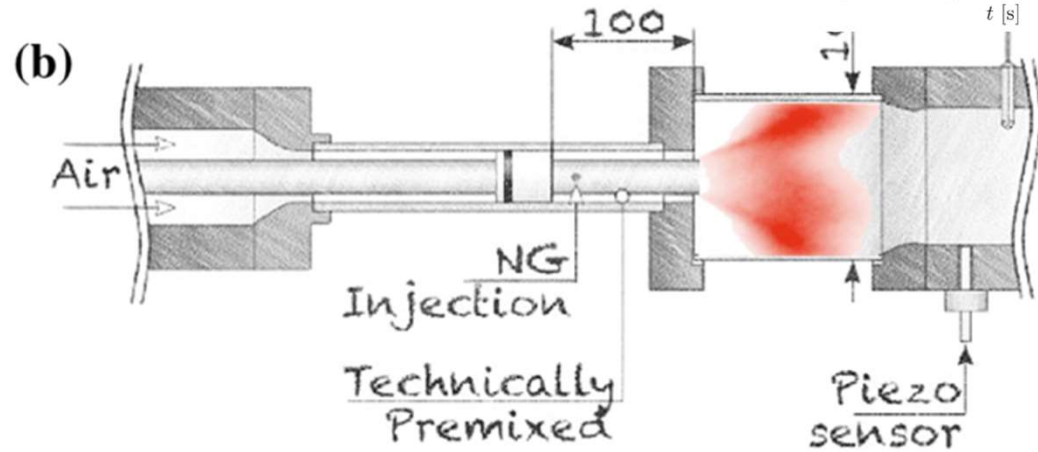
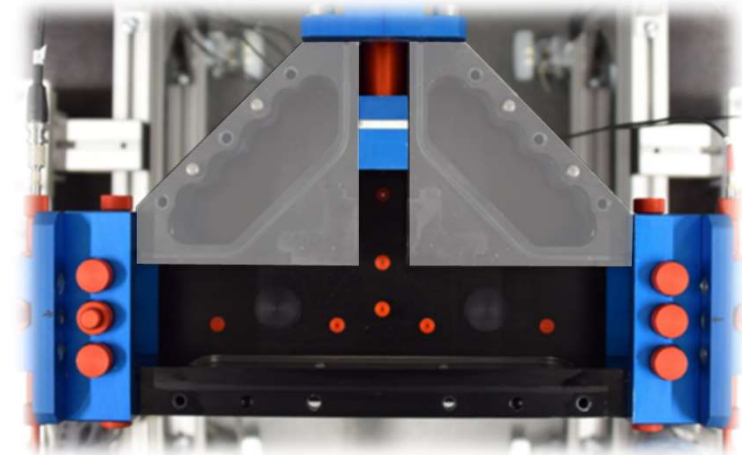
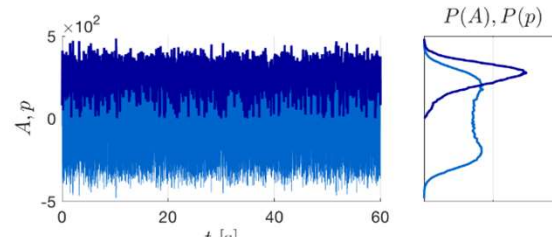
➤ Need for a repeatability

- Pay attention to the boundary conditions!!

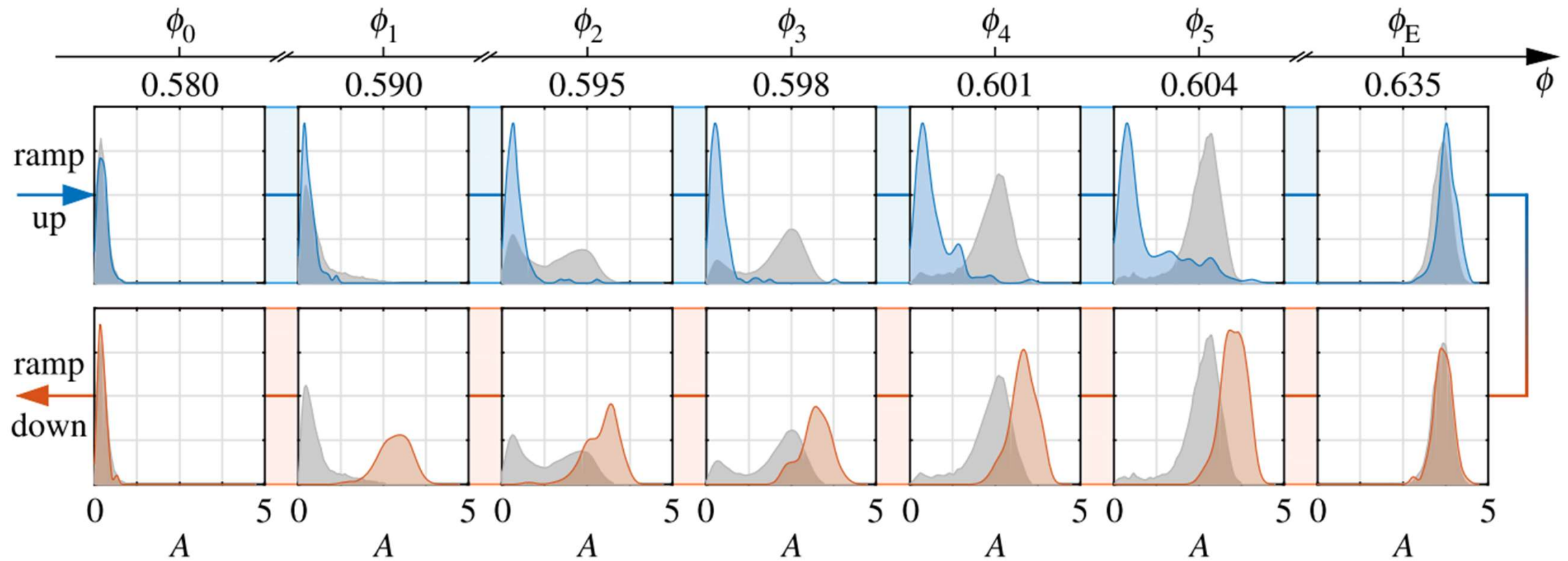
Bonciolini, G., Ebi, D., Doll, U., Weilenmann, M., & Noiray, N. (2019). Effect of wall thermal inertia upon transient thermoacoustic dynamics of a swirl-stabilized flame. *Proceedings of the Combustion Institute*, 37(4), 5351-5358.

- Check sensors regularly
- Make sure to document every little detail!

Amplitude maps

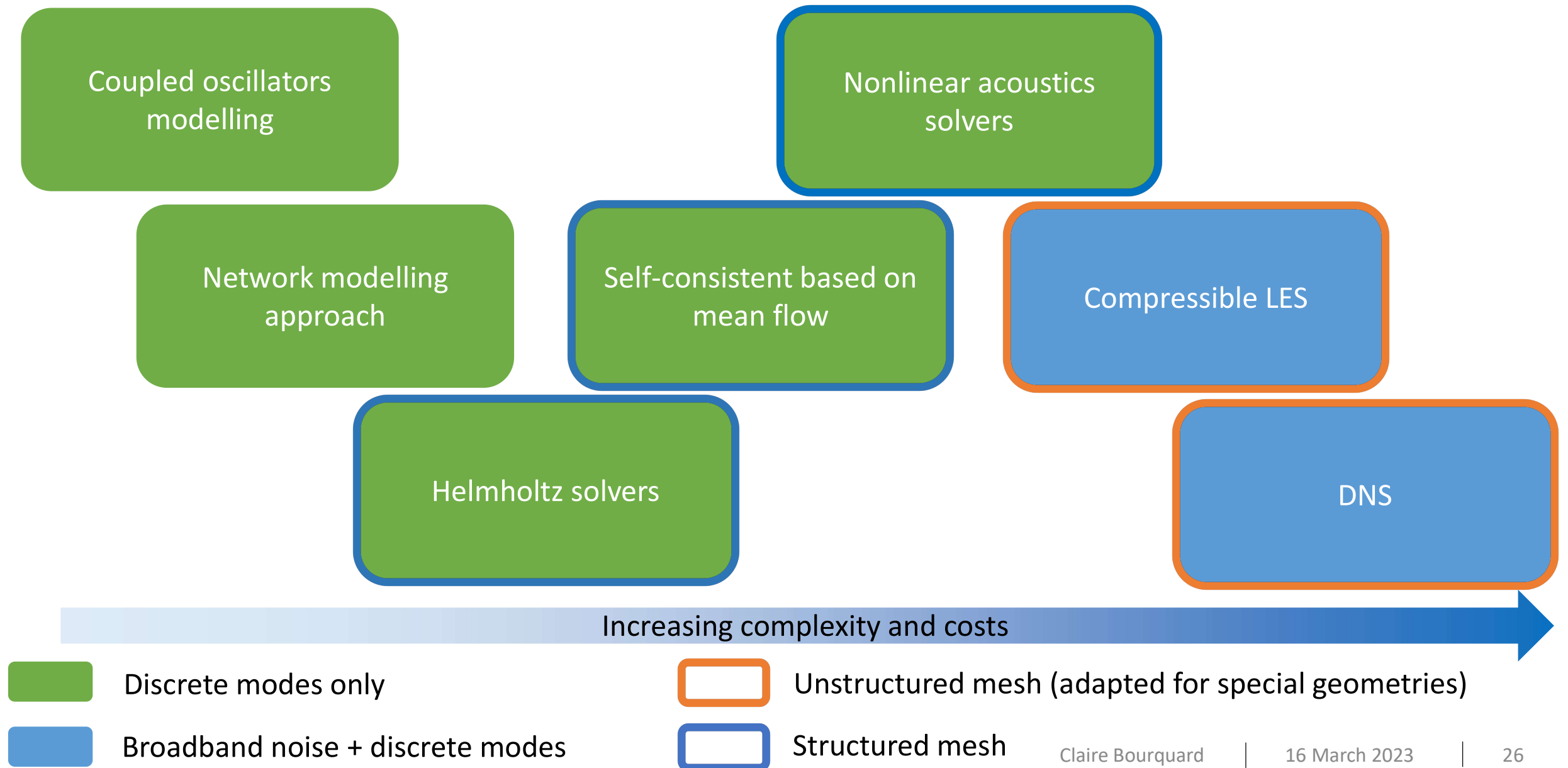


Subcritical characterization: ramping



Low order modeling

From low-order models to full DNS...



Why do we want to keep developing low-order models?


“While the sheer scale of the data generated by large-scale simulations will require new methods for data analysis and data visualization, it is our view that suitable theoretical formulations and reduced models will be even more important in future.”

Lele, Nichols. (2014) A second golden age of aeroacoustics? Philosophical Transactions of the Royal Society A 372, 20130321.

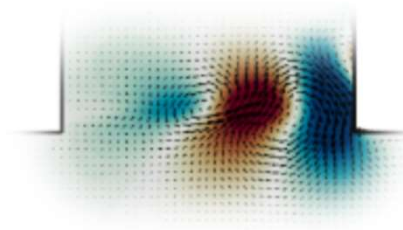
How many oscillators do I need?

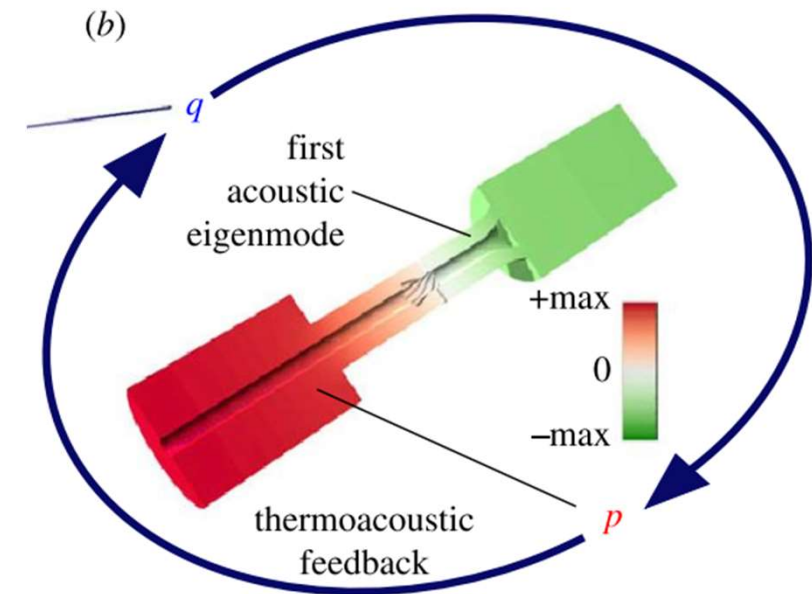
- As many as systems that you can model separately!

Acoustic response of the deep cavity:


$$f_a \simeq \frac{(2n - 1)c}{4L} \quad (\text{here } \frac{3}{4}\text{-wave, } n=2)$$

Hydrodynamic response of the shear layer:

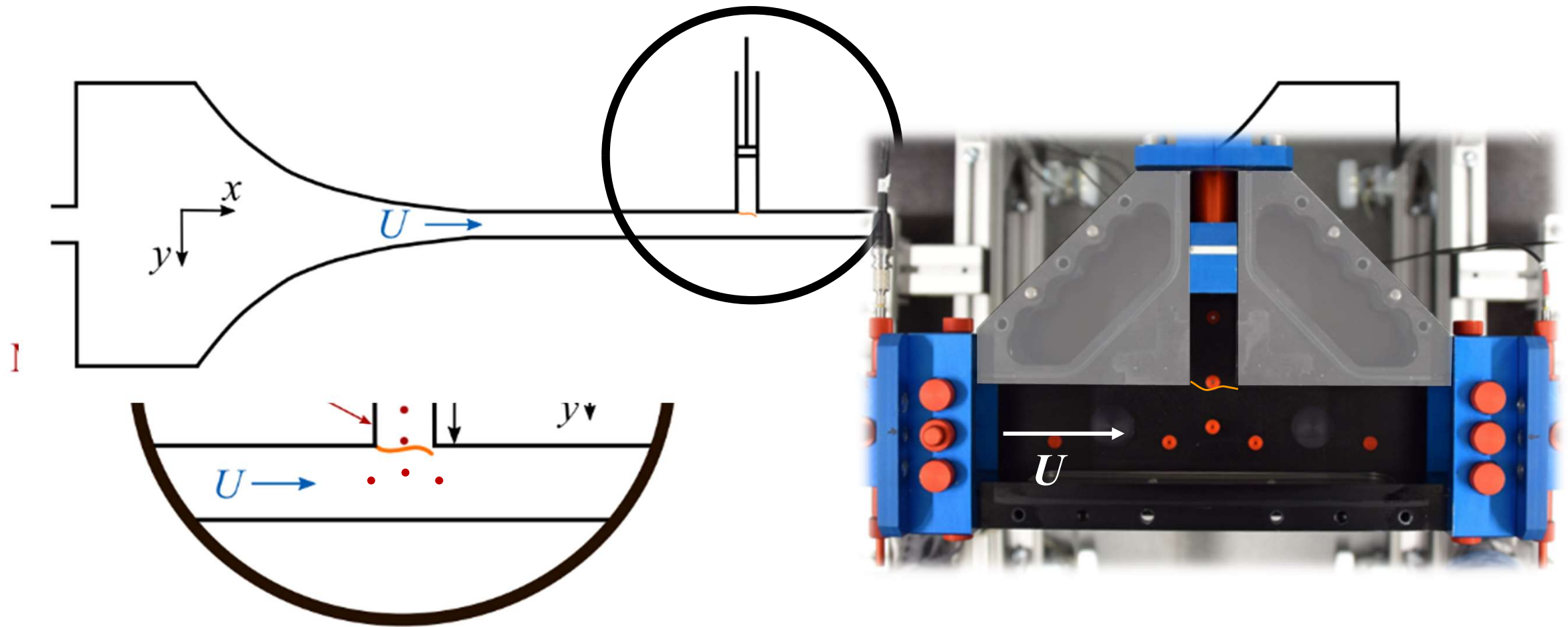
$$f_h \simeq \frac{nU}{2W}$$




The example of the aero-acoustic instability:

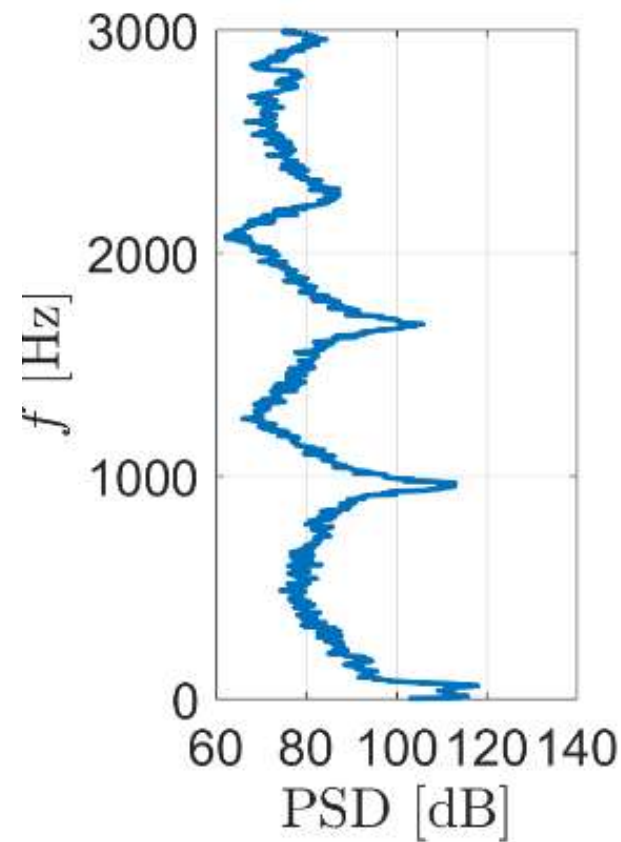
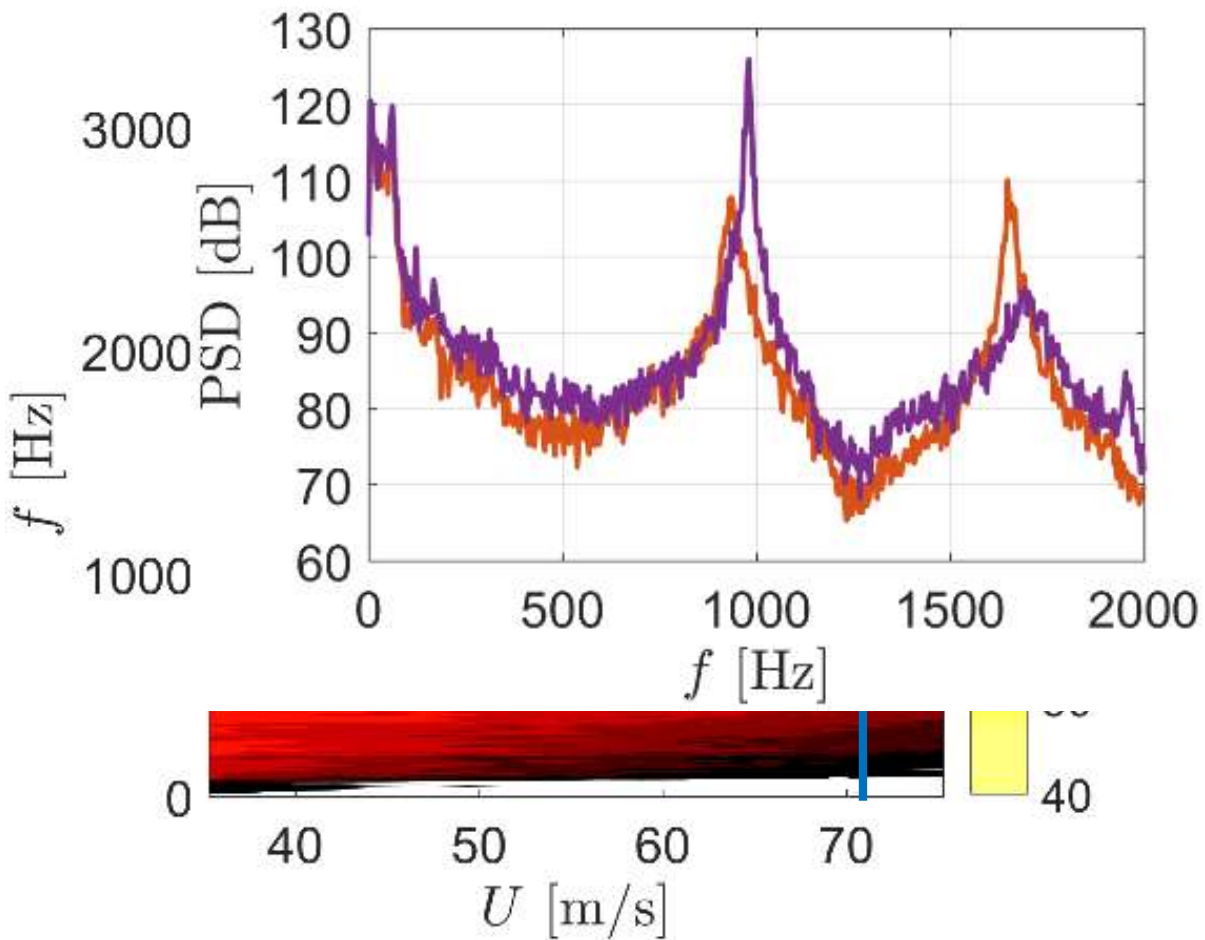
- How to determine coupling terms
- How to determine sources of nonlinearity
- How to model nonlinearities?

Introducing our aeroacoustic instability: experimental setup

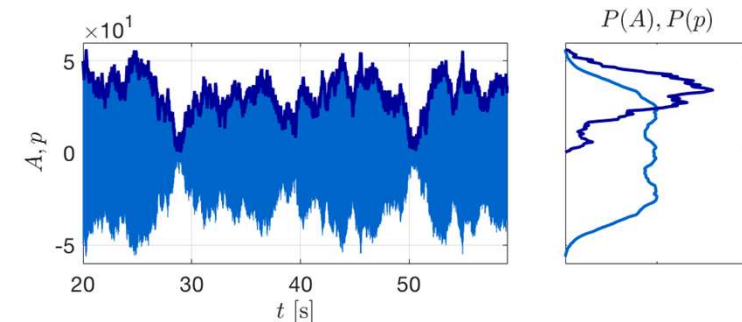
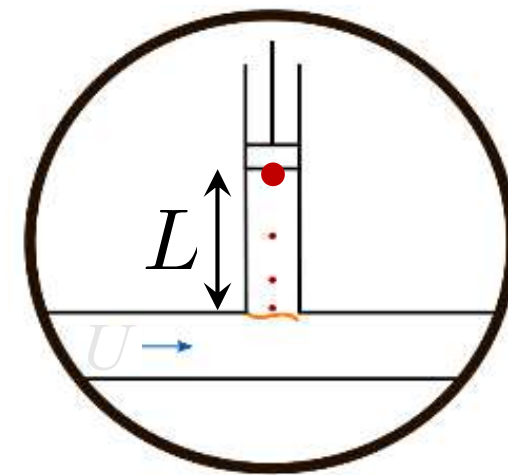


The aeroacoustic instability is characterized acoustically

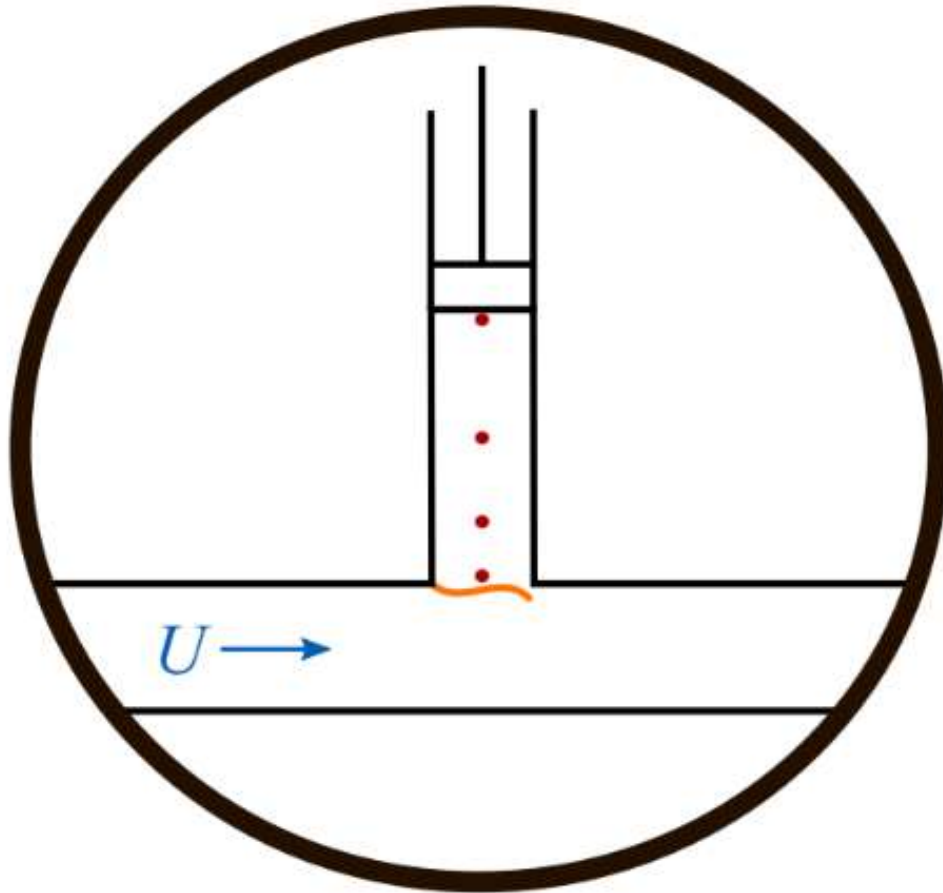
$U = 74 \text{ m/s}$
 $U = 63.5 \text{ m/s}$ $U = 74 \text{ m/s}$



$L = 250 \text{ mm}$



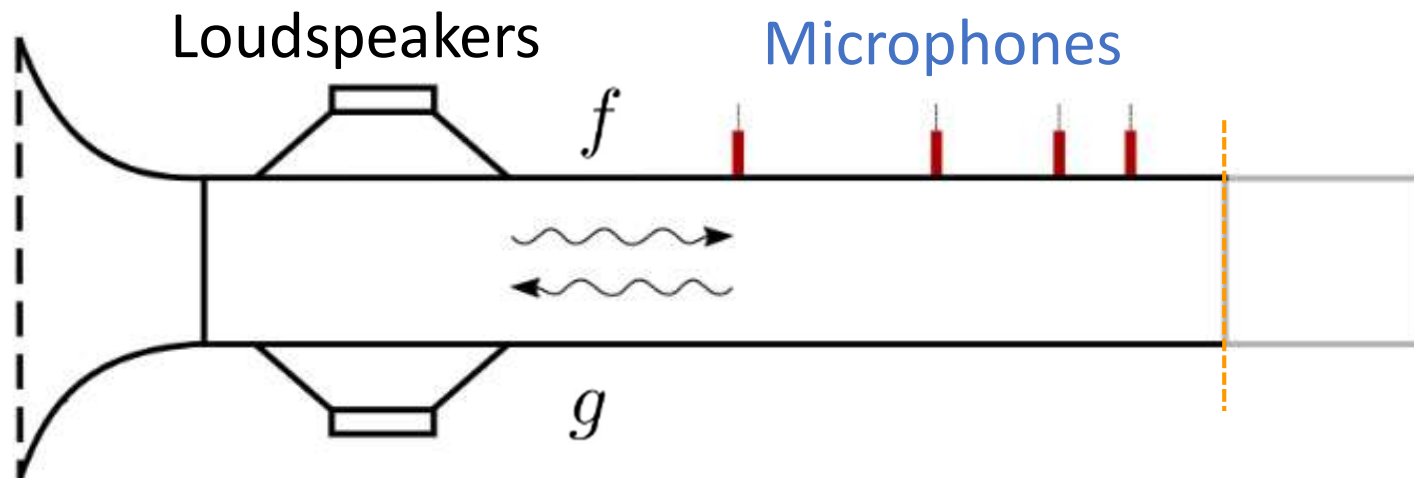
The acoustic responses are measured separately



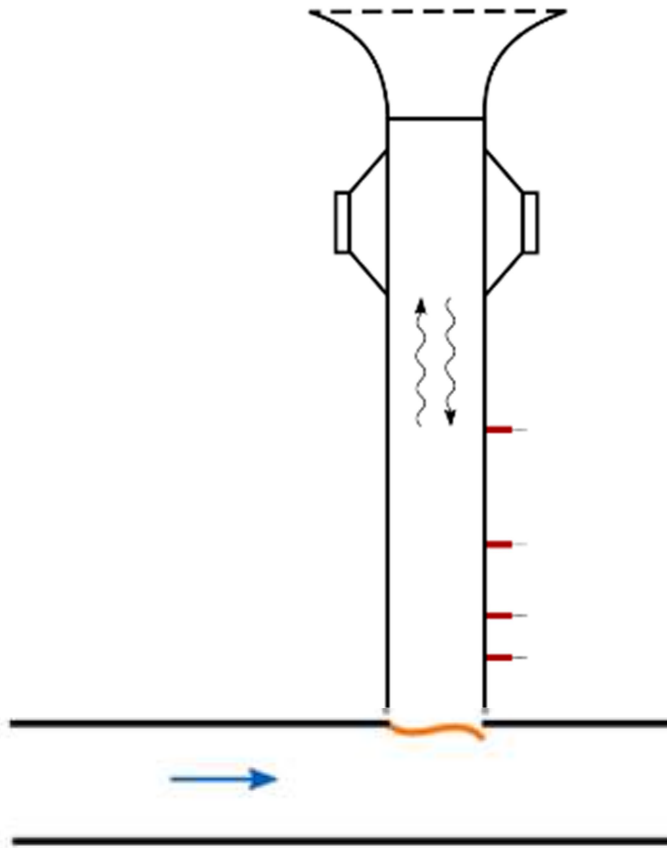
Impedance matching at the meeting plane:

$$Z = \frac{\hat{p}}{\hat{u}}$$

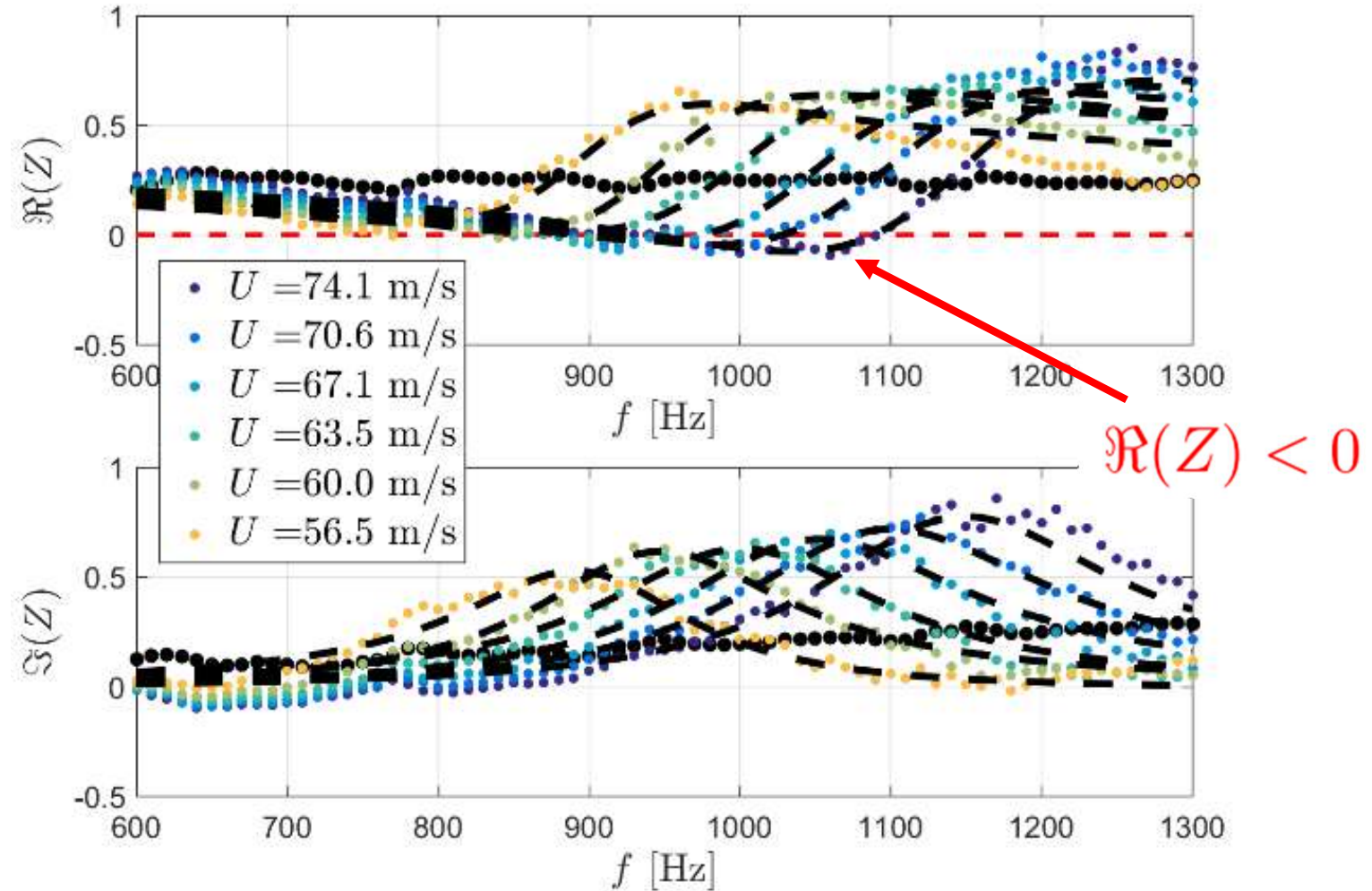
The acoustic response is measured with Multi-Microphone Method



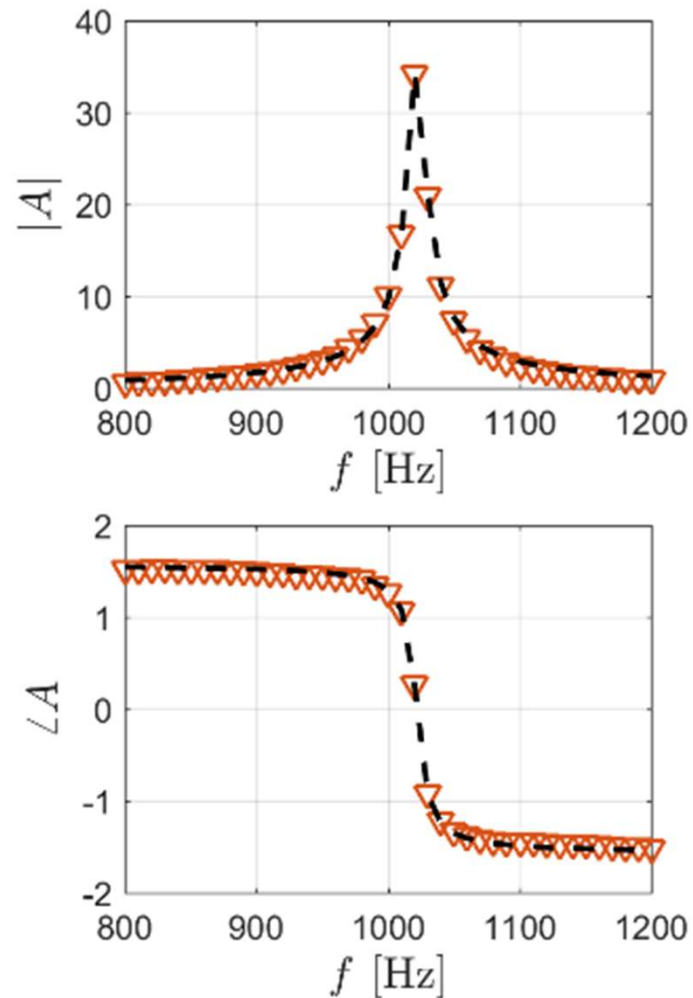
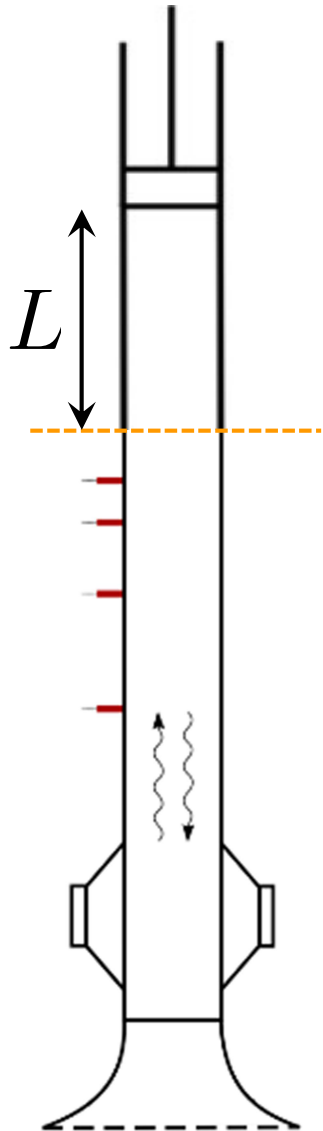
The acoustic response of the Shear Layer is measured



$$Z_{SL}(s) = \frac{\hat{p}}{\hat{u}} = n \frac{s^2 + 2ms + \omega_l^2}{s^2 + 2ds + \omega_h^2}$$



The acoustic response of the deep cavity is measured



$$A = 1/Z$$

$$A_{DC}(s) = \frac{\hat{u}}{\hat{p}} = -\frac{\gamma s}{s^2 + 2\alpha s + \omega_a^2}$$

$s = i\omega$ is the Laplace variable

$$Z_Q = \frac{\rho L}{2} \cdot \frac{s^2 + \frac{2R}{\rho L}s + \omega_Q^2}{s}$$

The coupled system is built from the two blocks

$$\left. \begin{aligned} Z_{SL}(s) &= \frac{\hat{p}}{\hat{u}} = n \frac{s^2 + 2ms + \omega_l^2}{s^2 + 2ds + \omega_h^2} \\ A_{DC}(s) &= \frac{\hat{u}}{\hat{p}} = -\frac{\gamma s}{s^2 + 2\alpha s + \omega_a^2} \end{aligned} \right\} \begin{array}{l} \text{Time} \\ \text{domain} \end{array} \rightarrow \begin{cases} \ddot{p} + 2d \dot{p} + \omega_h^2 p = n(\ddot{u} + 2m \dot{u} + \omega_l^2 u) \\ \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p} \end{cases}$$

Substituting \ddot{u}

$$\begin{cases} \ddot{p} + 2\beta \dot{p} + \omega_h^2 p = \mu \dot{u} + \sigma u \\ \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p} \end{cases}$$

With $\beta = (2d + n\gamma)/2$, $\mu = 2n(m - \alpha)$ and $\sigma = n(\omega_l^2 - \omega_a^2)$

Linear eigenvalues compare well with experiments

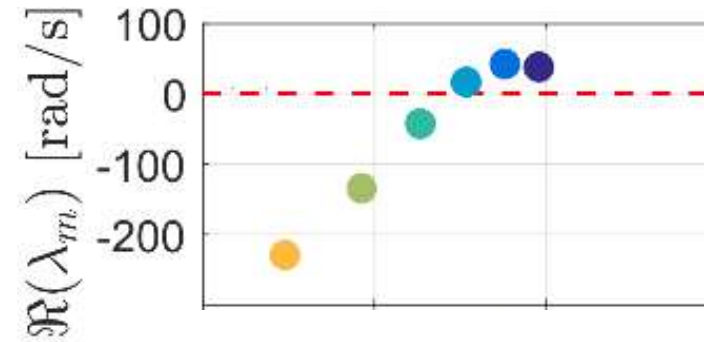
$$\begin{cases} \ddot{p} + 2\beta \dot{p} + \omega_r^2 p = \mu \dot{u} + \sigma u \\ \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p}, \end{cases}$$

Using $\mathbf{x} = (u, p)^T$

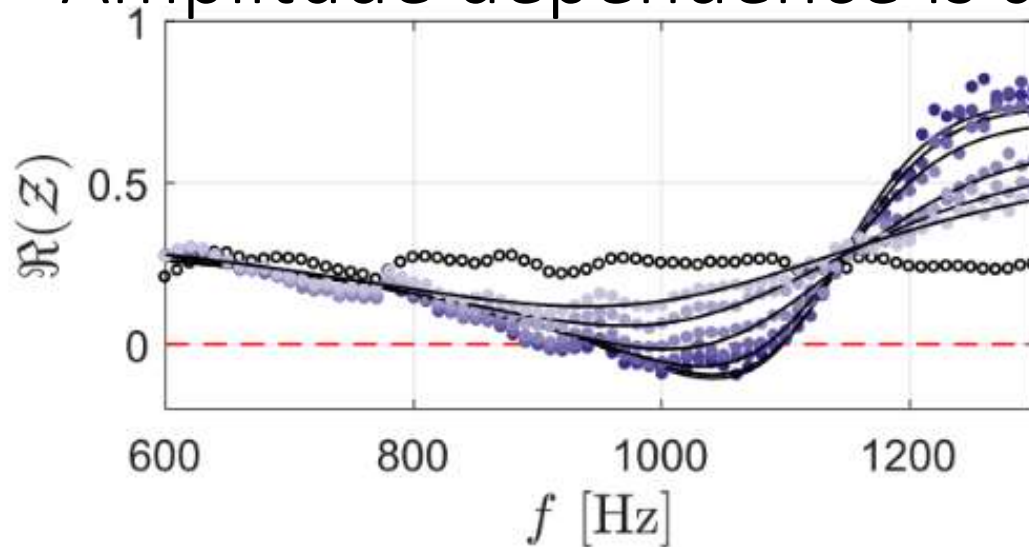
$$\underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}}_M \ddot{\mathbf{x}} + \underbrace{\begin{bmatrix} 2\beta & -\mu \\ \gamma & 2\alpha \end{bmatrix}}_D \dot{\mathbf{x}} + \underbrace{\begin{bmatrix} \omega_r^2 & -\sigma \\ 0 & \omega_a^2 \end{bmatrix}}_K \mathbf{x} = 0$$

Eigenvalues given by:

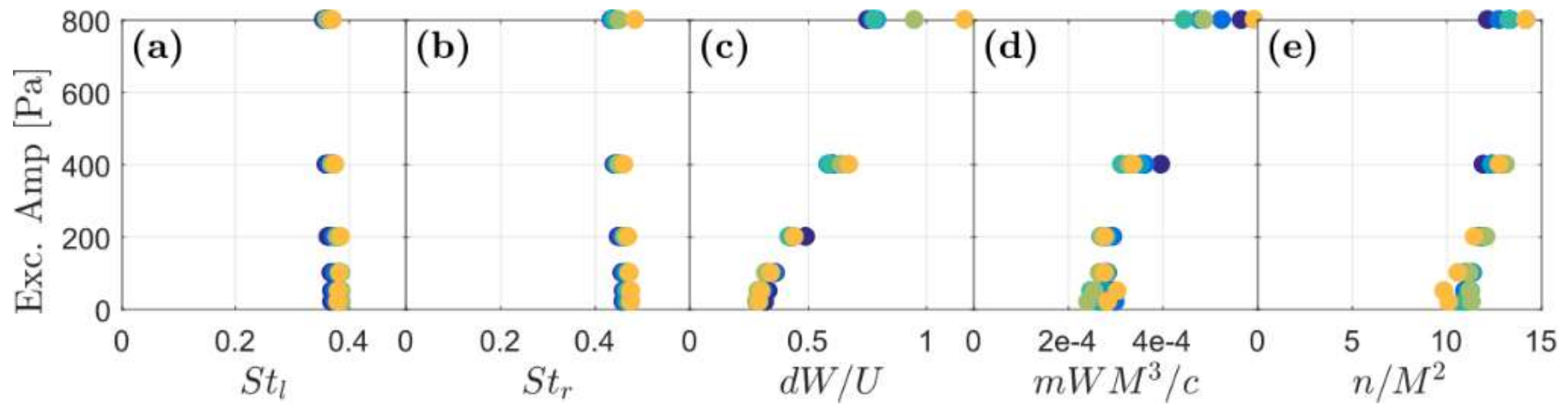
$$\det(s^2 M + sG + K) = 0.$$



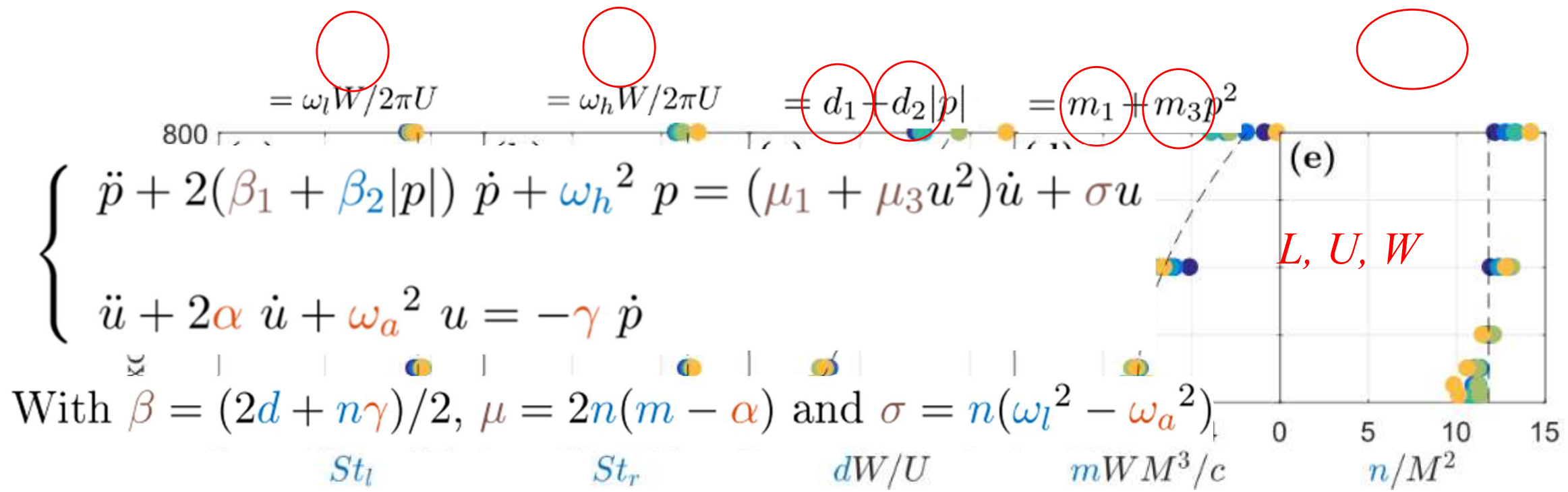
Amplitude dependence is also measured



$$Z_{SL}(s) = \frac{\hat{p}}{\hat{u}} = n \frac{s^2 + 2ms + \omega_l^2}{s^2 + 2ds + \omega_h^2}$$

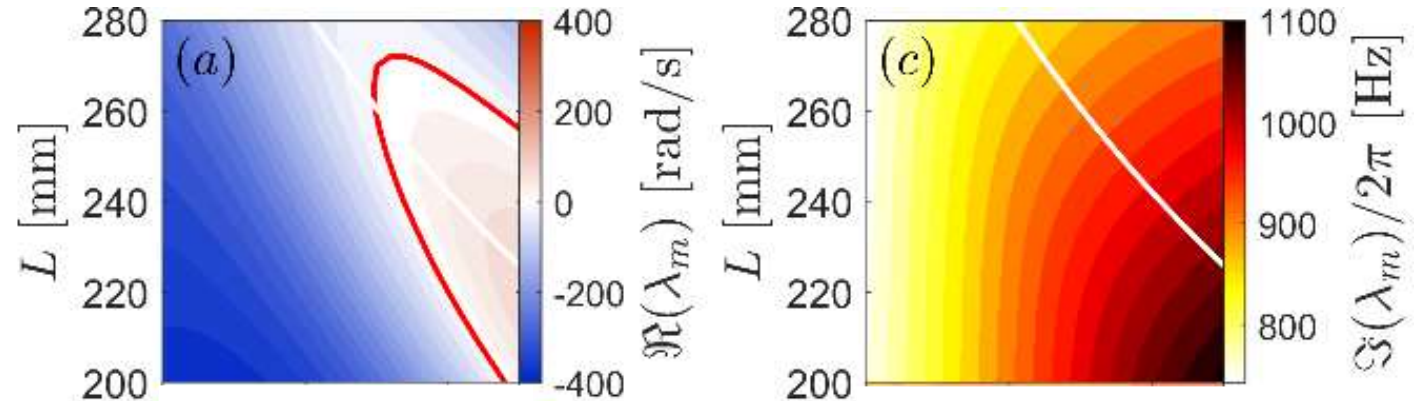


Scaling laws allow the derivation of nonlinear model



Full linear stability map

$$\begin{cases} \ddot{p} + 2(\beta_1 + \beta_2 |p|) \dot{p} + \omega_h^2 p = (\mu_1 + \mu_2 u^2) \dot{u} + \sigma u \\ \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p} \end{cases}$$



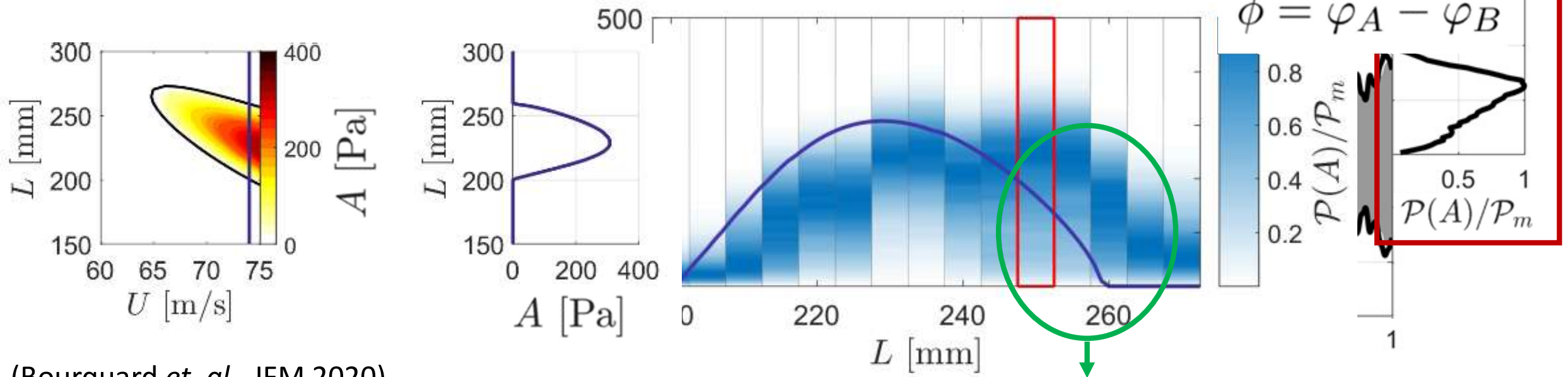
Limit cycle amplitude estimation

$$\begin{cases} \ddot{p} + 2(\beta_1 + \beta_2|p|) \dot{p} + \omega_h^2 p = (\mu_1 + \mu_3 u^2) \dot{u} + \sigma u \\ \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p} \end{cases}$$

Averaging:

$$\begin{cases} p = A \cos(\omega t + \varphi_A) \\ u = B \cos(\omega t + \varphi_B) \end{cases}$$

A, B slowly varying

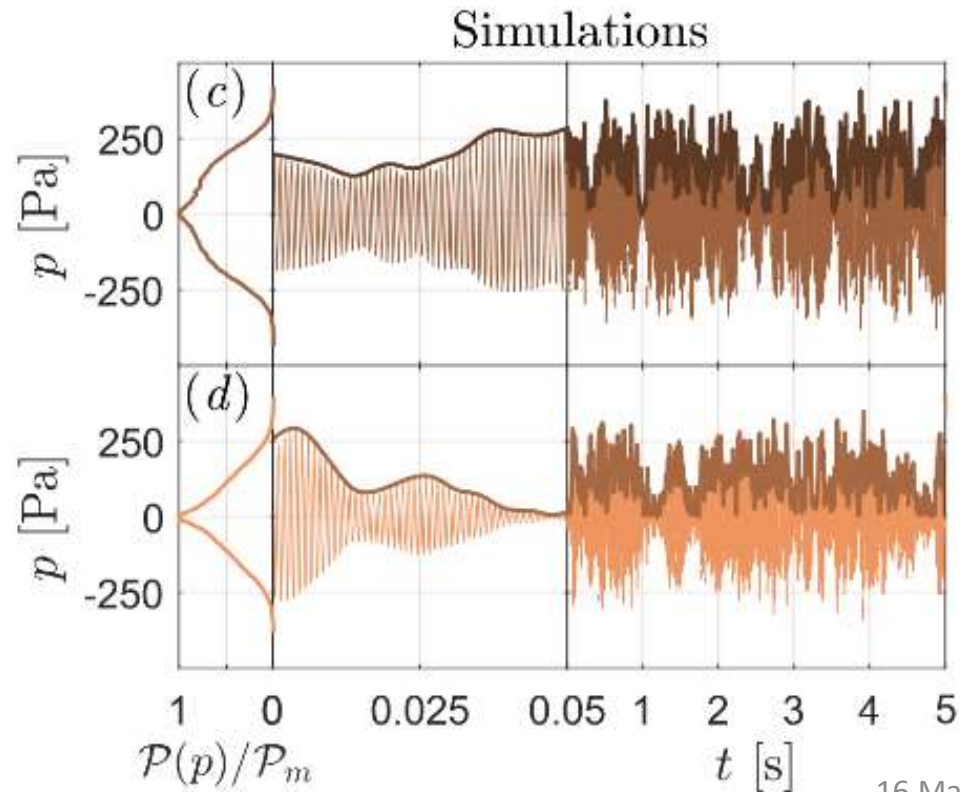
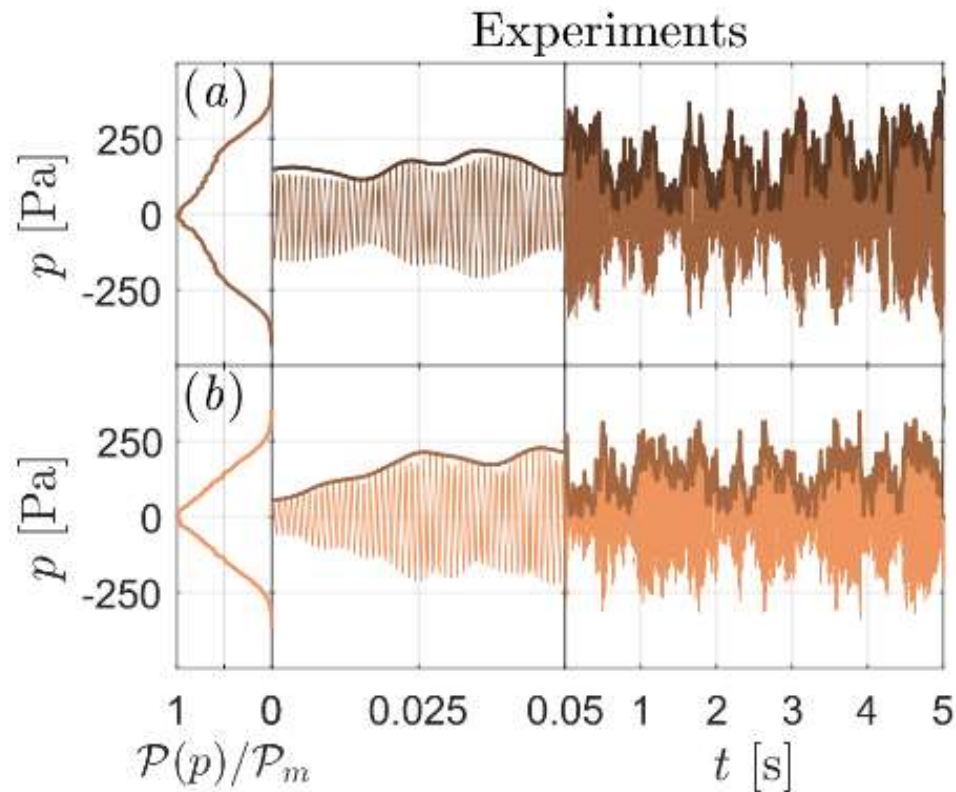


(Bourquard *et. al.*, JFM 2020)

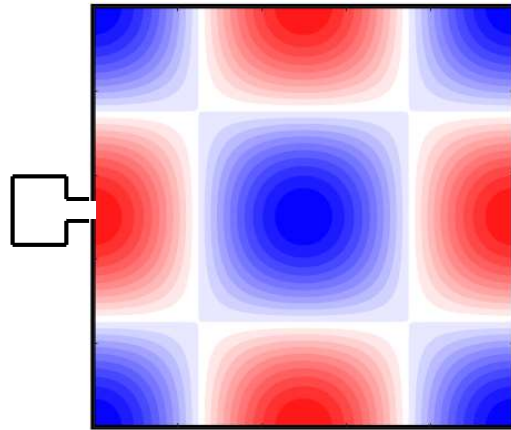
Could be modelled using: $\ddot{\eta} - (2\nu + \kappa\eta^2)\dot{\eta} + \omega_0^2\eta = 0$

Simulation of nonlinear system with multiplicative colored noise:
Intermittency is reproduced!

$$\left\{ \begin{array}{l} \ddot{u} + 2\alpha \dot{u} + \omega_a^2 u = -\gamma \dot{p} \\ \ddot{p} + 2(\beta_1 + \beta_2|p|) \dot{p} + \omega_h^2 p = (\mu_1 + \mu_3 u^2)\dot{u} + \sigma u. \end{array} \right. \quad U = \bar{U}(1 + \chi(t))$$



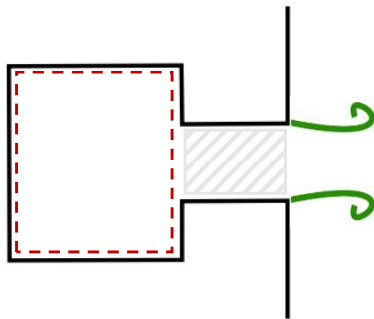
Nonlinearity terms: Helmholtz damper example



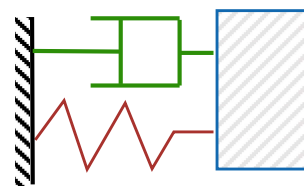
$$\dot{p} = \rho_n l \ddot{u} + \frac{\rho_v c^2 a}{V_h} u + \rho_n \zeta \bar{u} \dot{u}$$

$$p(t, \mathbf{x}) \simeq \eta(t) \psi(\mathbf{x})$$

$$\Theta = \psi(\mathbf{x}_d)$$

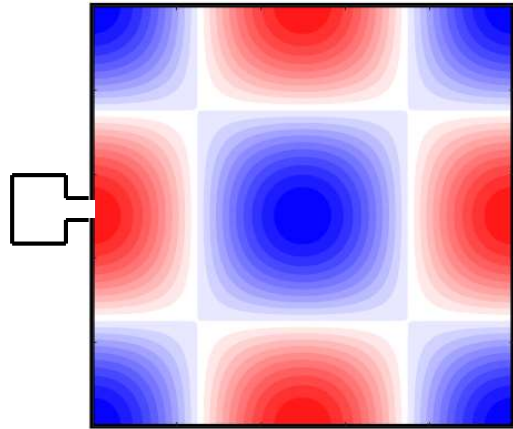


$$\ddot{u} + \frac{\zeta \bar{u}}{l} \dot{u} + \omega_d^2 u = \frac{\Theta}{\rho_n l} \dot{\eta}$$

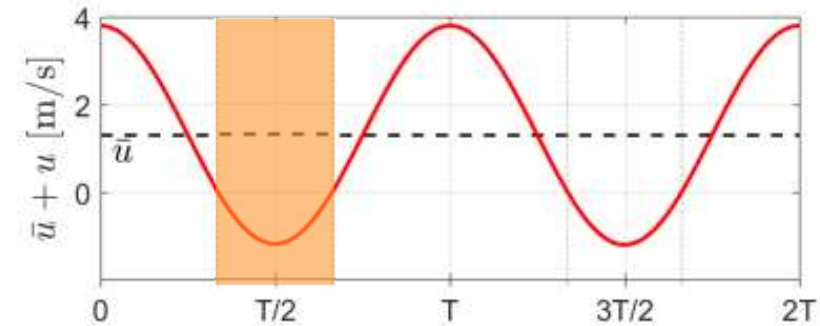


$$\text{with } \omega_d = c \sqrt{\frac{a}{V_h l}} \sqrt{\frac{\rho_v}{\rho_n}}$$

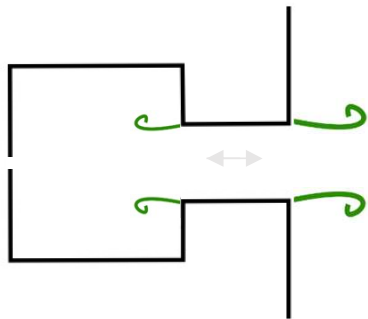
Nonlinearity terms: Helmholtz damper example



$$\ddot{u} + \frac{\zeta \bar{u}}{l} \dot{u} + \omega_d^2 u = \frac{\Theta}{\rho_n l} \dot{\eta}$$



Reverse flow



Damping term

$$\bar{u} \Rightarrow |\bar{u} + u|$$

Conclusion / Takeaway

- You are able to extract and interpret basic probability density functions of various nonlinear dynamical systems
- You know the different sources of intermittency
- You have an idea on how to model coupled oscillators with nonlinearity

Now's your turn to play!

References:

Bourquard, C., Faure-Beaulieu, A., & Noiray, N. (2021). Whistling of deep cavities subject to turbulent grazing flow: intermittently unstable aeroacoustic feedback. *Journal of Fluid Mechanics*, 909, A19.

Bonciolini, G., Faure-Beaulieu, A., Bourquard, C., & Noiray, N. (2021). Low order modelling of thermoacoustic instabilities and intermittency: flame response delay and nonlinearity. *Combustion and Flame*, 226, 396-411.

Pedergrana, T., Bourquard, C., Faure-Beaulieu, A., & Noiray, N. (2021). Modeling the nonlinear aeroacoustic response of a harmonically forced side branch aperture under turbulent grazing flow. *Physical Review Fluids*, 6(2), 023903.

Bonciolini, G., Ebi, D., Boujo, E., & Noiray, N. (2018). Experiments and modelling of rate-dependent transition delay in a stochastic subcritical bifurcation. *Royal Society open science*, 5(3), 172078.

Bonciolini, G., & Noiray, N. (2019). Bifurcation dodge: avoidance of a thermoacoustic instability under transient operation. *Nonlinear dynamics*, 96, 703-716.

And references therein...

Acknowledgements

Thanks to:

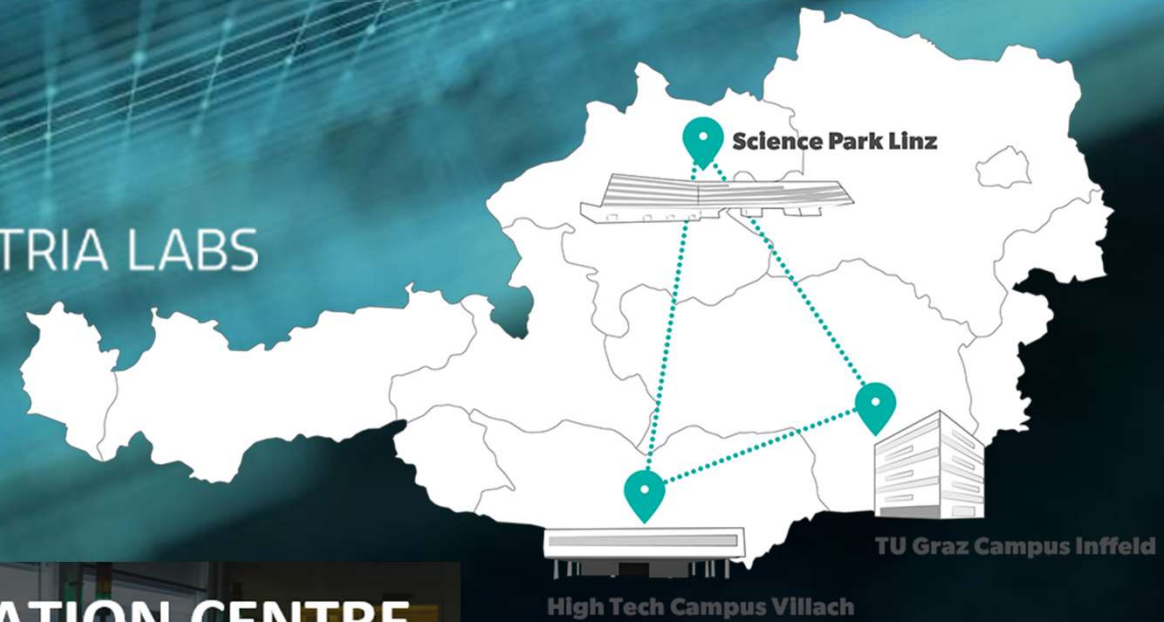
- Prof. Dr. Nicolas Noiray, PhD supervisor
- Prof. Dr. Outi Supponen, Postdoc group leader

- **Dr. Giacomo Bonciolini**
- Dr. Markus Weilenmann
- Dr. Yuan Xiong
- Dr. Abel Faure-Beaulieu
- Dr. Luigi Miniero

Students:

- Stefan Hiltbrand
- Denise Mühlethaler
- Emile Pecquet

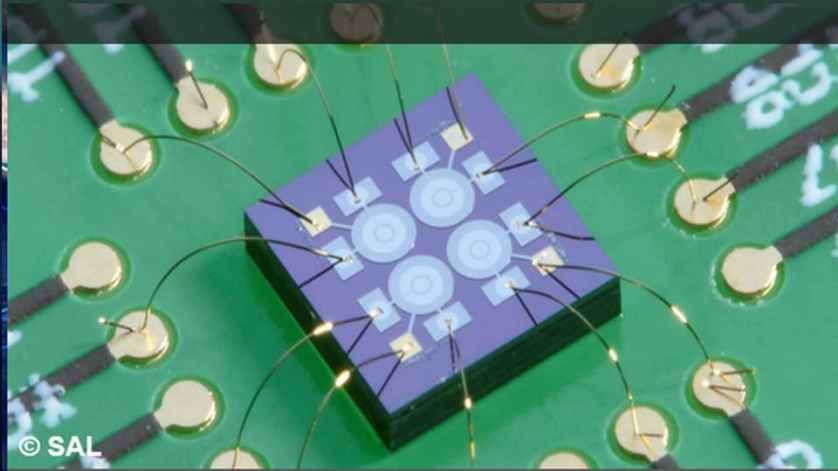




MEMS-based solutions for sensory applications
piezoelectric, optical & magnetic innovative sensors

MICROSYSTEMS

novel solutions for MEMS devices



SAL μnFABRICATION CENTRE

>1400m² state-of-the-art microfabrication facility

-  ISO 5 300 m² + ISO 7 100 m²
NEW ISO 4 1000 m² (Q4-2023)
-  8-inch capability
-  μFabrication
Advanced piezo thin film technology
-  Characterization
-  Design and modelling expertise
-  Attractive environment

16 March 2023

claire.bourquard@silicon-austria.com

Thanks for your attention!

Questions?